# An Iterative CN-Leapfrog Scheme Based Hybrid Implicit–Explicit Discontinuous Galerkin Finite-Element Time-Domain Method for Analysis of Multiscale Problems

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Abstract - The discontinuous Galerkin finite-element time-domain (DG-FETD) method with the ability to deal with unstructured meshes is well suited to analyze the multiscale system. However the DG-FETD method with explicit integration schemes is constrained by stability conditions that can be very restrictive upon highly fine meshes. The hybrid implicit-explicit Crank-Nicolson (CN) leapfrog scheme is effective in solving this problem; but because of using CN scheme, the inversion of a large sparse matrix must be calculated at each time step in the fine regions. The hybrid implicitexplicit iterative CN leapfrog scheme is introduced to improve the computational efficiency which can form a block diagonal matrix. The leapfrog scheme is employed for electrically coarse regions and iterative CN scheme for electrically fine ones. The numerical examples have demonstrated the validity and efficiency of the method.

*Index Terms* — Crank-Nicolson, discontinuous Galerkin finite-element time-domain method, multi-scale.

## I. INTRODUCTION

When handling the multiscale electromagnetic simulations in transient electromagnetic analysis, such as electromagnetic interference and electromagnetic compatibility problems, traditional methods face great challenges because of small size meshes in the fine regions. The finite-element time-domain (FETD) method is widely used because of its flexibility in geometric modeling, but it must calculate a large sparse matrix inversion at each time step [1]. Then the discontinuous Galerkin method has been proposed and combined with the FETD method called discontinuous Galerkin finite-element time-domain (DG-FETD) method [2]-[4]; Numerical fluxes are introduced to impose the tangential continuity of the electrical and magnetic fields at the interfaces between adjacent elements. Central flux [5, 6] and upwind flux [7, 8] are the commonly used ways. The explicit leapfrog scheme for DG-FETD method can make the mass matrix block-diagonal and it is convenient for matrix inversion and parallel computing rather than solve a huge matrix system as conventional FETD method [9-12]. But the size of the time step of the explicit leapfrog DG-FETD is limited by the spatial discretization of the simulation domain according to the CFL condition which will lead to produce a large number of simulation steps and reduce the computation efficiency. Generally, a discretized multiscale system usually contains both electrically coarse meshes and fine meshes. Because of the constraint of Courant-Friedrichs-Levy (CFL) stability condition [13], the time step increments for electrically fine meshes may be much less than those for electrically coarse meshes when the explicit leapfrog time integration scheme is employed. According to this circumstance, hybrid implicit-explicit Crank-Nicolson (CN) leapfrog scheme have been proposed to get a higher computational efficiency [14]. The implicit CN scheme used in fine regions can make the system unconditionally stable but also require solving large matrices equations which will destroy the original powerful ability of DG-FETD. Therefore, an iterative CN leapfrog scheme DG-FETD is proposed, which can not only make system unconditionally stable but also maintain the advantage of DG-FETD.

In this paper, an iterative CN leapfrog scheme is introduced to analyze multiscale electromagnetic

problems. The leapfrog scheme is employed for electrically coarse regions and iterative Crank-Nicholson scheme [15] for electrically fine ones. In the paper, an iterative CN leapfrog scheme is first introduced with poor convergence. To solve the poor convergence problem, a modified iterative CN leapfrog scheme is further presented to speed up the convergence.

The paper is organized as follows. The basic theory and formulations of the hybrid implicit–explicit iterative CN leapfrog scheme for DG-FETD is presented in Section II. The numerical results are given to demonstrate the validity of proposed method in Section III, and the conclusion is drawn in Section IV.

#### **II. THEORY AND FORMULATIONS**

#### A. DG-FETD spatial semi-discrete formulation

The implementation steps of the DG-FETD method include choice of the governing equation, grid discretization and imposing the tangential continuity of the electrical and magnetic fields at the interfaces between adjacent elements. In this paper, first order Maxwell's curl equations based on E and H are employed and the model is discretized by tetrahedral meshes, central flux scheme is employed. Considering the time-dependent Maxwell's curl equations for a linear, lossless, isotropic and non-dispersive medium, the electric field E and the magnetic field H can be described as:

$$\varepsilon \frac{\partial \boldsymbol{E}}{\partial t} = \nabla \times \boldsymbol{H} \,, \tag{1}$$

$$u\frac{\partial \boldsymbol{H}}{\partial t} = -\nabla \times \boldsymbol{E} , \qquad (2)$$

where  $\varepsilon$  represents the permittivity and  $\mu$  denotes the permeability. The electric and magnetic fields can be expanded by Whiney edge elements [16] as:

$$\boldsymbol{E} = \sum_{j} \boldsymbol{W}_{ej} \boldsymbol{e}_{j}, \quad \boldsymbol{H} = \sum_{j} \boldsymbol{W}_{hj} \boldsymbol{h}_{j}. \tag{3}$$

The curl-conforming vector basis functions  $W_{ej}$  and

 $W_{hj}$  are chosen to discretize the *E* field and *H* field respectively. Then  $e_j$  and  $h_j$  are the unknown coefficients. The Galerkin's weak forms of Maxwell's equations can be described as:

$$\iiint_{V} \boldsymbol{W}_{ei} \cdot \boldsymbol{\varepsilon} \, \frac{\partial \boldsymbol{E}}{\partial t} dV - \iiint_{V} \nabla \times \boldsymbol{W}_{ei} \cdot \boldsymbol{H} dV = \iint_{S} \boldsymbol{W}_{ei} \cdot (\mathbf{n} \times \boldsymbol{H}) dS,$$
(4)

$$\iiint_{V} \mathbf{W}_{hi} \cdot \mu \frac{\partial \mathbf{H}}{\partial t} dV + \iiint_{V} \nabla \times \mathbf{W}_{hi} \cdot \mathbf{E} dV = \iint_{S} \mathbf{W}_{hi} \cdot (\mathbf{n} \times \mathbf{E}) dS.$$
(5)

The central flux is employed for each element to impose the tangential continuity of the electric and magnetic fields at the interfaces between adjacent elements and the expression is:

$$\mathbf{n} \times \boldsymbol{H}\Big|_{\partial V} = \frac{1}{2} \mathbf{n} \times (\boldsymbol{H} + \boldsymbol{H}^{+})\Big|_{\partial V}, \qquad (6)$$

$$\mathbf{n} \times \boldsymbol{E} \Big|_{\partial V} = \frac{1}{2} \mathbf{n} \times (\boldsymbol{E} + \boldsymbol{E}^{+}) \Big|_{\partial V}, \qquad (7)$$

where E and H represent the electric and magnetic fields of the elements within sub-domain V,  $E^+$  and  $H^+$  represent electric and magnetic fields of the adjacent elements within the neighboring sub-domain V+. By substituting (6) and (7) into (4) and (5), the final spatial semi-discrete DG-FETD formulations can be converted into a matrix equation as follows:

$$\mathbf{T}_{ee} \frac{\partial \boldsymbol{e}}{\partial t} = \mathbf{P}_{eh} \boldsymbol{h} + \mathbf{S}_{eh}^{+} \boldsymbol{h} , \qquad (8),$$

$$\mathbf{T}_{hh}\frac{\partial \boldsymbol{h}}{\partial t} = \mathbf{P}_{he}\boldsymbol{e} + \mathbf{S}_{he}^{+}\boldsymbol{e} , \qquad (9)$$

where  $\mathbf{T}_{ee}$ ,  $\mathbf{T}_{hh}$ ,  $\mathbf{P}_{eh}$ ,  $\mathbf{P}_{he}$ ,  $\mathbf{S}_{eh}^+$  and  $\mathbf{S}_{he}^+$  are the sparse matrices, e and h are the unknown vectors. The matrix elements are defined as:

$$\begin{split} [\mathbf{T}_{ee}]_{ij} &= \varepsilon \iiint_{V} \mathbf{W}_{ei} \cdot \mathbf{W}_{ej} dV, \\ [\mathbf{T}_{hh}]_{ij} &= \mu \iiint_{V} \mathbf{W}_{hi} \cdot \mathbf{W}_{hj} dV, \\ [\mathbf{P}_{eh}]_{ij} &= \iiint_{V} \nabla \times \mathbf{W}_{ei} \cdot \mathbf{W}_{hj} dV + \frac{1}{2} \iint_{S} \mathbf{W}_{ei} \cdot \mathbf{n} \times \mathbf{W}_{hj} dS, \\ [\mathbf{P}_{he}]_{ij} &= -\iiint_{V} \nabla \times \mathbf{W}_{hi} \cdot \mathbf{W}_{ej} dV - \frac{1}{2} \iint_{S} \mathbf{W}_{hi} \cdot \mathbf{n} \times \mathbf{W}_{ej} dS, \\ [\mathbf{S}_{eh}^{+}]_{ij} &= \frac{1}{2} \iint_{S} \mathbf{W}_{ei} \cdot \mathbf{n} \times \mathbf{W}_{hj}^{+} dS, \\ [\mathbf{S}_{he}^{+}]_{ij} &= -\frac{1}{2} \iint_{S} \mathbf{W}_{hi} \cdot \mathbf{n} \times \mathbf{W}_{ej}^{+} dS. \end{split}$$

#### **B.** Iterative CN-leapfrog scheme

When dealing with multiscale electromagnetic problems, very small size meshes will appear in fine regions of the model. Though explicit leapfrog scheme of the DG-FETD method makes the mass matrix blockdiagonal and it is convenient for matrix inversion and parallel computing. But the size of the time step of the explicit leapfrog DG-FETD is limited by the spatial discretization of the simulation domain according to the CFL condition which lead to produce a large number of simulation steps and reduce the computation efficiency. In contrast, the implicit time step schemes are proved to be unconditionally stable with large time step intervals but require solving large matrix equations. Therefore, hybrid implicit-explicit CN leapfrog scheme can be attractive in multi-scale electromagnetic simulations. However, the implicit-explicit CN leapfrog DG-FETD lost the block diagonal characteristic because of using implicit CN scheme which lead to a mass matrix of DG-FETD. In this section, an iterative CN Leapfrog scheme is proposed to deal with the above problems which can not only maintain the block diagonal characteristic of the DG-FETD method but also improve the computational efficiency.

The proposed hybrid iterative CN Leapfrog scheme divides the whole computational domain into the coarse region marked by region 1 and the fine region marked by region 2, [1]. In region 1, explicit leapfrog scheme is employed to DG-FETD method and the Eq. (8), Eq. (9) above can be changed into:

$$\mathbf{T}_{hh} \frac{h^{n+\frac{1}{2}} - h^{n-\frac{1}{2}}}{\Delta t} = \mathbf{P}_{he} e^n + \frac{1}{2} (\mathbf{S}_{he} e^n + \mathbf{S}_{he}^+ e^n) , \qquad (10)$$

$$\mathbf{T}_{ee} \frac{e^{n+1} - e^n}{\Delta t} = \mathbf{P}_{eh} h^{n+\frac{1}{2}} + \frac{1}{2} (\mathbf{S}_{eh} h^{n+\frac{1}{2}} + \mathbf{S}_{eh}^{+} h^{n+\frac{1}{2}}) .$$
(11)

Where  $\Delta t$  represents the time step size and can be expressed as:

$$\Delta t \leq \frac{h_{\min}}{2v_{\max}(p+1)^2},$$

where  $h_{\min}$  is the minimum length of the mesh,  $v_{\max}$  is the propagation speed of the wave in the object, P is the order of the base function.

In region 2, iterative CN scheme is applied to DG-FETD method and the Eq. (8), Eq. (9) can be expressed as:

$$\mathbf{T}_{hh} \cdot \frac{h^{n+1} - h^n}{\Delta t} = \mathbf{P}_{he} \cdot \frac{e^{n+1} + e^n}{2} + \mathbf{S}_{he} \cdot \frac{e^{n+1} + e^n}{2} + \mathbf{S}_{he}^{+} \cdot \frac{e^{n+1} + e^n}{2},$$
(12)
$$\mathbf{T}_{ee} \cdot \frac{e^{n+1} - e^n}{\Delta t} = \mathbf{P}_{eh} \cdot \frac{h^{n+1} + h^n}{2} + \mathbf{S}_{eh} \cdot \frac{h^{n+1} + h^n}{2} + \mathbf{S}_{eh}^{+} \cdot \frac{h^{n+1} + h^n}{2}.$$
(13)

The proposed scheme can be described by the following steps:

- Step 1. Assume that the correct overall distribution of the electromagnetic fields at the time of  $n\Delta t$  is known.
- Step 2. In region 1, the leapfrog scheme for DG-FETD as Eq. (10) and Eq. (11) calculate the electric and magnetic fields at the time of  $(n + \frac{1}{n})\Delta t$ .

$$\mathbf{T}_{\mathbf{h}\mathbf{h}\mathbf{l}} \cdot \frac{h_{\mathbf{h}}^{n+\frac{1}{2}} - h_{\mathbf{h}}^{n}}{\Delta t / 2} = \mathbf{P}_{\mathbf{h}\mathbf{c}\mathbf{l}} \cdot e_{\mathbf{l}}^{n} + \mathbf{S}_{\mathbf{h}\mathbf{c}\mathbf{l}} \cdot e_{\mathbf{l}}^{n} + \mathbf{S}_{\mathbf{h}\mathbf{c}\mathbf{l}}^{+} \cdot e_{\mathbf{l}}^{n} + \mathbf{S}_{\mathbf{h}\mathbf{c}\mathbf{l}}^{+} \cdot e_{\mathbf{l}}^{n} + \mathbf{S}_{\mathbf{h}\mathbf{c}\mathbf{l}}^{+} \cdot e_{\mathbf{l}}^{n}$$

$$\left[\mathbf{T}_{ee1} \cdot \frac{\mathbf{c}_{1} - \mathbf{c}_{1}}{\Delta t / 2} = \mathbf{P}_{eh1} \cdot \mathbf{h}_{1}^{+2} + \mathbf{S}_{eh1} \cdot \mathbf{h}_{1}^{+2} + \mathbf{S}_{eh1}^{+} \cdot \mathbf{h}_{1}^{+2} + \mathbf{S}_{eh12}^{+} \cdot \mathbf{h}_{2}^{n}\right]$$
(14)

Step 3. In region 2, CN scheme for DG-FETD as Eq. (12) and Eq. (13) calculate the electric and magnetic fields at the time of  $(n+1)\Delta t$ :

$$\begin{cases} \mathbf{T}_{\mathbf{h}\mathbf{h}2} \cdot \frac{h_{2}^{n+1} - h_{2}^{n}}{\Delta t} \\ = \mathbf{P}_{\mathbf{h}\mathbf{c}2} \cdot \frac{e_{2}^{n+1} + e_{2}^{n}}{2} + \mathbf{S}_{\mathbf{h}\mathbf{c}2} \cdot \frac{e_{2}^{n+1} + e_{2}^{n}}{2} + \mathbf{S}_{\mathbf{h}\mathbf{c}2}^{n+1} \cdot \frac{e_{2}^{n+1} + e_{2}^{n}}{2} + \mathbf{S}_{\mathbf{h}\mathbf{c}21}^{n+\frac{1}{2}} \\ \mathbf{T}_{\mathbf{c}\mathbf{c}2} \cdot \frac{e_{2}^{n+1} - e_{2}^{n}}{\Delta t} \\ = \mathbf{P}_{\mathbf{c}\mathbf{h}2} \cdot \frac{h_{2}^{n+1} + h_{2}^{n}}{2} + \mathbf{S}_{\mathbf{c}\mathbf{h}2} \cdot \frac{h_{2}^{n+1} + h_{2}^{n}}{2} + \mathbf{S}_{\mathbf{c}\mathbf{h}2}^{n+1} + \frac{h_{2}^{n}}{2} + \mathbf{S}_{\mathbf{c}\mathbf{h}2^{n+1}} + \frac{h_{2}^{n}}{2} + \mathbf{S}_$$

Equation (15) can be converted into a matrix equation:

$$\begin{bmatrix} \mathbf{T}_{ee2} & -\Delta t \frac{\mathbf{P}_{eh2} + \mathbf{S}_{eh2}}{2} \\ -\Delta t \frac{\mathbf{P}_{he2} + \mathbf{S}_{he2}}{2} & \mathbf{T}_{hh2} \end{bmatrix} \begin{bmatrix} e_2^{n+1} \\ h_2^{n+1} \end{bmatrix} + \mathbf{S}_{eh2}^{+} \begin{bmatrix} e_2^{n+1} \\ h_2^{n+1} \end{bmatrix} + \mathbf{S}_{he2}^{+} \begin{bmatrix} e_2^{n+1} \\ h_2^{n+1} \end{bmatrix}$$

$$= \begin{bmatrix} \mathbf{T}_{ee2} & \Delta t \frac{\mathbf{P}_{eh2} + \mathbf{S}_{eh2} + \mathbf{S}_{eh2}^{+}}{2} \\ \Delta t \frac{\mathbf{P}_{he2} + \mathbf{S}_{he2} + \mathbf{S}_{he2}^{+}}{2} & \mathbf{T}_{hh2} \end{bmatrix} \begin{bmatrix} e_2^{n} \\ h_2^{n} \end{bmatrix}$$

$$+ \begin{bmatrix} \Delta t \mathbf{S}_{he21}^{+} & \Delta t \mathbf{S}_{eh21}^{+} \end{bmatrix} \begin{bmatrix} e_1^{n+\frac{1}{2}} \\ h_1^{n+\frac{1}{2}} \end{bmatrix},$$

$$(16)$$

because  $S_{eh2}^{+}$  and  $S_{he2}^{+}$  present the matrices of the adjacent element in region 2 which destroy the block diagonal characteristic of the mass matrix,  $S_{eh2}^{+}$  and  $S_{he2}^{+}$  are moved to the right-hand side of the equation to ensure the mass matrix of the left-hand side is a block diagonal matrix:

$$\begin{bmatrix} \mathbf{T}_{ee2} & -\Delta t \frac{\mathbf{P}_{eh2} + \mathbf{S}_{eh2}}{2} \\ -\Delta t \frac{\mathbf{P}_{he2} + \mathbf{S}_{he2}}{2} & \mathbf{T}_{hh2} \end{bmatrix} \begin{bmatrix} e_2^{n+1} \\ h_2^{n+1} \end{bmatrix}$$

$$= \begin{bmatrix} \mathbf{T}_{ee2} & \Delta t \frac{\mathbf{P}_{eh2} + \mathbf{S}_{eh2} + \mathbf{S}_{eh2}^{+}}{2} \\ \Delta t \frac{\mathbf{P}_{he2} + \mathbf{S}_{he2} + \mathbf{S}_{he2}^{+}}{2} & \mathbf{T}_{hh2} \end{bmatrix} \begin{bmatrix} e_2^{n} \\ h_2^{n} \end{bmatrix}$$

$$+ \begin{bmatrix} \Delta t \mathbf{S}_{he21}^{+} \end{bmatrix} \begin{bmatrix} e_1^{n+\frac{1}{2}} \\ h_1^{n+\frac{1}{2}} \end{bmatrix} + \begin{bmatrix} \Delta t \frac{\mathbf{S}_{eh2}^{+}}{2} \\ \Delta t \frac{\mathbf{S}_{eh2}^{+}}{2} \end{bmatrix} \begin{bmatrix} e_2^{n+1} \\ h_2^{n+1} \end{bmatrix}$$
(17)

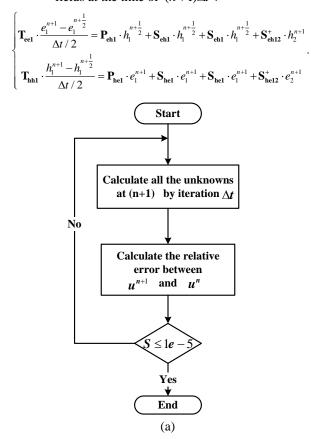
The linear system of Eq. (17) will be solved iteratively and can be expressed as:

$$[\mathbf{T}]u_{i,k+1}^{n+1} = [\mathbf{S}_1]u_i^n + [\mathbf{S}_2]u_j^n + [\mathbf{S}_3]u_{j,k}^{n+1},$$

where subscript i represents the *i*th element, j represents the *j*th adjacent element, subscript k denotes the *k*th iteration. The initial value of  $u_{j,0}^{n+1}$  in the right hand side of the equation is set to be the previous time step value  $u_j^n$  as  $u_{j,0}^{n+1} = u_j^n$ . After a few iterations for the solution of the  $u_{i,k+1}^{n+1}$ , the error can be acceptable and then go to the next step.

Iterative number for convergence determines the speedup effect of the method during the implementation. In this paper, the global iterative method is first proposed. By one-time iteration, all of the unknowns are obtained and compared with the results in the previous step. Root mean square error (RMSE) is calculated to determine whether the iteration is over or not. If the iteration is over, it will go to the next step. However, this method we first proposed with disadvantage of poor convergence performance will lead to increasing the iterative steps and enlarge the time step size. To solve this problem, a modified iterative CN method is further proposed. For this method, electromagnetic fields of each element are calculated by iteration and are updated immediately until all the elements are calculated and updated. Then RMSE is calculated. The procedure of the two proposed methods is given as Fig. 1 below.

Step 4. In region 1, CN scheme is employed in Eq. (6) and Eq. (7) to calculate the electric and magnetic fields at the time of  $(n+1)\Delta t$ :



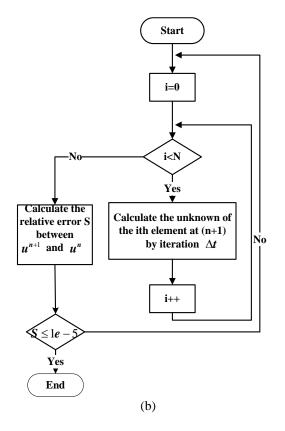


Fig. 1. (a) Flow chart of the iterative CN scheme, and (b) flow chart of the modified iterative CN scheme.

# III. NUMERICAL RESULTS AND DISCUSSION

In order to verify the accuracy and efficiency of the proposed method, two numerical examples are analyzed. The first example is a rectangular cavity with the size of 10mm×5mm×15mm. The number of the discretized tetrahedron is 1771 and the number of unknowns is 19015 and the time step size is  $1.17 \times 10^{-13}$  s which is five times as large as that of the leapfrog scheme. A modulated Gaussian pulse is selected as the excitation and the center frequency is 18GHz. The convergence speed is compared between iterative CN DG-FETD and modified iterative CN DG-FETD when both of the methods require 500 time steps. As shown in Fig. 2, the modified iterative CN DG-FETD can speed up the convergence effectively. The parameters of CN DG-FETD and iterative CN DG-FETD are also compared as shown in Table 1, which further demonstrates that the convergence speed of modified iterative CN method is superior to the iterative CN method and computational time of modified iterative CN method is much less than CN method.

The second example is a metal cylinder cavity loaded with a dielectric cylinder as shown in Fig. 3. The radius of the metal cylinder is 0.5m and the height is 1m .The radius of the dielectric cylinder is 0.05m, the height is 0.02m and the relative permittivity is 4.0. A modulated Gaussian pulse is selected as the excitation in y direction with the center frequency of 230MHz. The number of the total discretized tetrahedron is 8464. The number of unknowns is 96089 with 14005 unknowns for the fine domain using CN method and 82084 unknowns for coarse domain using leapfrog method. The time step size is  $1.33 \times 10^{-11}$ s which is twice leapfrog time step size, Fig. 4 represents the transient scattering fields with two different method. Good agreement can be shown from the results obtained by the above different ways. Furthermore, Table 2 exhibits computational cost of the above different methods which further demonstrate the efficiency and accuracy of the proposed method.

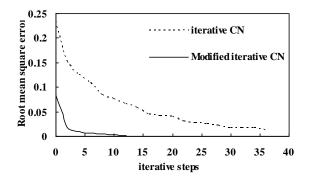


Fig. 2. Comparison of the convergence speed between two methods.

Table 1: Comparison of computational efficiency

Method	Number of Unknowns (CN)	Number of Unknowns (Leapfrog)	Iterative Steps	Iterative Time(s)
CN-leapfrog	14005	82084	5000	1104
Iterative CN-leapfrog	14005	82084	5000	650

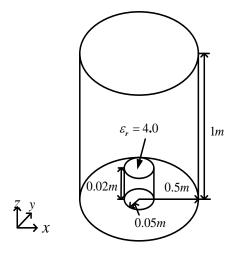


Fig. 3. A metal cylinder cavity loaded with a dielectric cylinder.

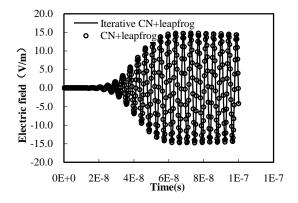


Fig. 4. Electric field in time domain calculated by the two methods.

Table 2: Comparison of computational efficiency				
Amplification of Time Step	Mean Convergence Step	Iterative Time(s)		
5	0	600		
5	35	415		
5	13	173		
	Amplification of Time	Amplification of TimeMean ConvergenceStepStep50535		

Table 2: Comparison of computational efficiency

#### **IV. CONCLUSION**

In the paper, a hybrid explicit-implicit iterative CNleapfrog scheme based DG-FETD method is proposed for analysis of multiscale problems. The scheme divides the whole computational domain into two types. The iterative CN scheme is used in the fine regions while the leapfrog scheme is used in the coarse regions. Compared with the existing CN scheme and CNleapfrog scheme, our scheme can not only enlarge the time step size but also ensure the mass matrix with the block diagonal characteristic. Numerical results show the accuracy and efficiency of the proposed iterative CN-leapfrog scheme DG-FETD.

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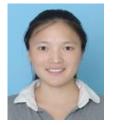
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