

# Dielectric Resonator Antenna Based Dual Port Multiple Input Multiple Output Antenna

Muhammad Zia Hameed<sup>1</sup>, Shabbir Majeed<sup>1</sup>, Rashid Saleem<sup>2</sup>,  
Muhammad Farhan Shafique<sup>3</sup>, and Sabih ur Rehman<sup>4</sup>

<sup>1,2</sup>Department of Electrical and Telecommunication Engineering  
University of Engineering and Technology, Taxila, 47050, Pakistan  
ziahameed47@gmail.com, shabbir.majeed@uettaxila.edu.pk, rashid.saleem@uettaxila.edu.pk

<sup>3</sup>Center for Advanced Studies in Telecom (CAST)  
COMSATS Institute of Information Technology (CIIT), Park Road, Chak Shahzad, Islamabad, 45550, Pakistan  
farhan.shafique@comsats.edu.pk

<sup>4</sup>School of Computing and Mathematics, Charles Sturt University (CSU), Australia

**Abstract** — This paper presents a Dielectric Resonator based dual frequency band Multiple Input and Multiple Output (MIMO) antenna for wireless communication. This antenna is designed for WLAN (5.5–5.8 GHz) and X-band (8–8.1 GHz) applications. A pair of DRAs is placed on a FR-4 substrate and is excited through microstrip feed lines placed on rear side of substrate. A via-less EBG structure is introduced to suppress the mutual coupling among DRAs. The measured isolation among the two antenna ports is 25 dB and 41 dB for 5.6 GHz and 8.05 GHz respectively. The overall dimension of the antenna is  $0.72 \lambda_0 \times 0.52 \lambda_0$  at lower resonant frequency. Simulated and measured results are in good agreement, which supports the potential application of the proposed antenna for high gain WLAN and X-band applications.

**Index Terms** — Dielectric Resonator Antenna (DRA), decoupling structure, Electromagnetic Band Gap (EBG), Multiple Input Multiple Output (MIMO).

## I. INTRODUCTION

MIMO system is the technology of choice in wireless communication to meet the high data rate and high diversity gain requirements [1]. Microstrip patch antennas are extensively reported for MIMO applications. However, these antennas are prone to high metallic losses and lesser radiation efficiency, especially at higher frequencies. Dielectric Resonator Antennas (DRAs) do not have these disadvantages. They have several distinct benefits as compared to microstrip patch antennas, such as high radiation efficiency, higher gain and low losses [2]. MIMO system performance is affected by undesired mutual coupling among the

radiating elements which is developed due to miniaturization of the antenna design. Different techniques such as the Defected Ground Structures (DGSs), Electromagnetic Band Gap (EBG) structures and Frequency Selective Surfaces (FSSs) [3, 4] are reported in the literature to enhance isolation between antenna elements for different MIMO systems. A split ground plane is another commonly reported solution to accomplish high isolation in MIM DRAs [5, 6]. Aperture-coupled and probe feedings in hybrid feeding mechanism can also be used to achieve high isolation [7]. However, the techniques presented in [5, 6, 7] make fabrication more complex and compromise the design compactness.

In this work, a compact dual band MIMO DRA is proposed for WLAN and X-band applications. DRAs are placed on a  $38.8 \text{ mm} \times 28 \text{ mm} \times 1.6 \text{ mm}$  FR-4 substrate. A via-less EBG structure has been used to enhance the isolation among the DRAs.

The rest of this paper is organized as follows: in Section II a discussion of proposed antenna design configuration is given, DRA resonant frequency and modal analysis are given in Section III, simulated and measured results are presented in Section IV, and finally Section V concludes the paper.

## II. ANTENNA DESIGN

The proposed design geometry is shown in Figs. 1 (a) and 1 (b) along with the dimensions. The proposed antenna is simulated and optimized in Ansys HFSS<sup>®</sup>. The realized MIMO design is shown in Figs. 2 (a) and 2 (b). The dimensions of the substrate are  $l_1 = 28 \text{ mm} \times w_1 = 38.8 \text{ mm} \times h_2 = 1.6 \text{ mm}$ , as shown in Fig. 1 (a). The

cylindrical DRAs are mounted on the top side of FR-4 substrate. These DRAs are made of Alumina with: dielectric constant,  $\epsilon_r$ , of 9.8; dielectric loss tangent,  $\tan \delta$  of 0.002; radius,  $r$  of 6.35 mm and height,  $h_1$  of 9 mm. The spacing between the DRAs is  $d_1 = 8.72$  mm. DRAs are proximity/couple-fed through two microstrip feed lines etched at the rear side of substrate, each of length  $l_3 = 22$  mm and width  $w_3 = 2.05$  mm. Feed lines are separated by a distance  $d_2 = 19$  mm.

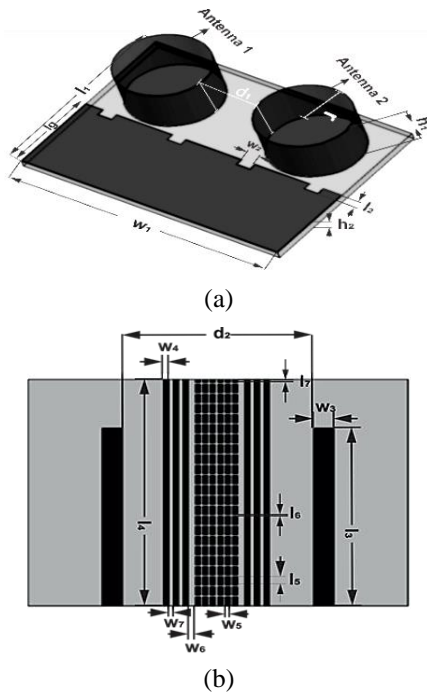


Fig. 1. MIMO DRA design: (a) front side and (b) back side.

A common ground plane arrangement is employed on the front side of substrate in the suggested MIMO design, as shown in Fig. 1 (a). The ground plane dimensions are  $l_g = 13.4$  mm  $\times$   $w_1 = 38.8$  mm. Rectangular shaped slits are imprinted in the top edge of the ground plane to improve impedance matching for the desired resonant frequencies. These rectangular slits have dimensions of  $l_2 = 1.1$  mm  $\times$   $w_2 = 2$  mm.

A via-less EBG structure is employed in this design to enhance isolation. This structure is imprinted on the back side of the substrate as shown in Fig. 1 (b).

The dimensions of each single rectangular block in via-less EBG structure are  $l_5 = 1$  mm  $\times$   $w_5 = 0.5$  mm. The spacing  $l_6$  between adjacent rectangular blocks is 0.25 mm. Furthermore, a pair of three vertical strips is placed on both sides of the via-less EBG structure. The dimensions of each strip are  $l_4 = 28$  mm  $\times$   $w_4 = 0.5$  mm. The spacing between adjacent strips is  $w_7 = 0.5$  mm and first strip is placed at a distance of  $w_6 = 0.75$  mm from the EBG structure.

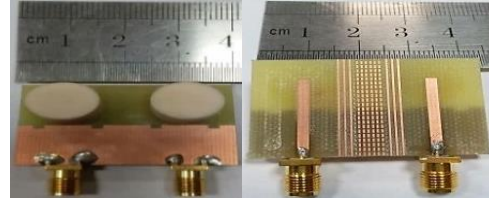


Fig. 2. Fabricated MIMO DRA: (a) front side and (b) back side.

### III. RESONANT FREQUENCY AND MODAL ANALYSIS OF DRA

The proposed DRA design has two resonant modes,  $HEM_{11\delta}$  and  $TM_{01\delta}$ . The first resonant mode is  $HEM_{11\delta}$  and it produces broadside radiation pattern, as shown in Fig. 3 and it can be theoretically verified with the following relation [9]:

$$f_o(HEM_{11\delta}) = \frac{c \times 6.324}{2\pi a \sqrt{\epsilon_r + 2}} \left( 0.27 + 0.36 \frac{a}{2h} + 0.02 \left( \frac{a}{2h} \right)^2 \right). \quad (1)$$

Where “a” is the radius of DR and “h” is the height of DR. The above equation is valid for  $0 \leq a/h \leq 6$ . The theoretical calculation of the resonant frequency from the above equation gives 5.53 GHz.

The second resonant mode is  $TM_{01\delta}$  and it offers end-fire radiation pattern, as shown in Fig. 4 and it can be theoretically calculated [9] as:

$$f_o(TM_{01\delta}) = \frac{c \sqrt{3.83^2 + \left( \frac{\pi a}{2h} \right)^2}}{2\pi a \sqrt{\epsilon_r + 2}}. \quad (2)$$

The above equation is valid for  $0.33 \leq a/h \leq 5$ . The theoretical calculation of the resonant frequency from the above equation gives 8.73 GHz.

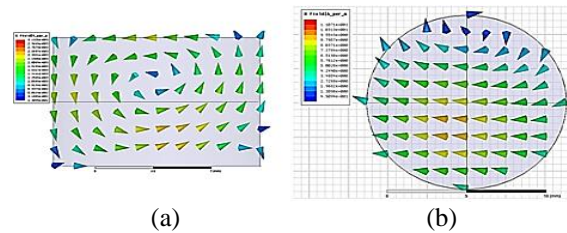


Fig. 3. First resonant mode  $HEM_{11\delta}$  of the DRA: (a) E-field pattern and (b) H-field pattern.

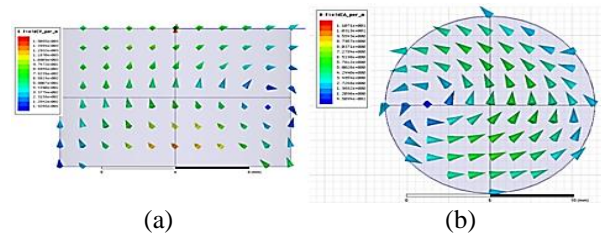


Fig. 4. Second resonant mode  $TM_{01\delta}$  of the DRA: (a) E-field pattern and (b) H-field pattern.

### IV. SIMULATED AND MEASURED RESULTS

#### A. S-parameters

Measured and simulated  $S_{11}$  and  $S_{12}$  results with and without decoupling structure are shown in Fig. 5. The  $S_{11}$  result shows that the suggested MIMO antenna design is well matched on 5.6 GHz and 8.05 GHz. The  $S_{12}$  result shows that more than 20 dB isolation is achieved between antennas, when the via-less EBG structure is introduced.

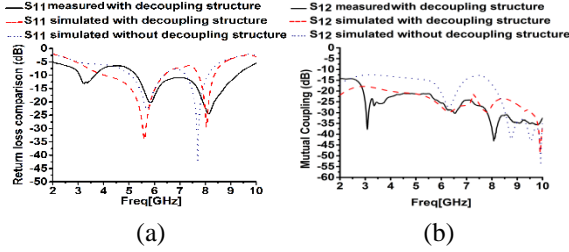


Fig. 5. Simulated and measured S-parameters of MIMO design: (a)  $S_{11}$  and (b)  $S_{12}$ .

#### B. Induction current suppression

The surface current density is plotted at 5.6 GHz and 8.05 GHz, as shown in Figs. 6 (a) and 6 (b). The  $J_{surf}$  plots show the undesired induced surface currents on ground plane and the feeding line of antenna, when the MIMO design is simulated without the decoupling structure. However, decoupling structure effectively suppresses the undesired surface currents, resulting in significant isolation between the antenna ports.

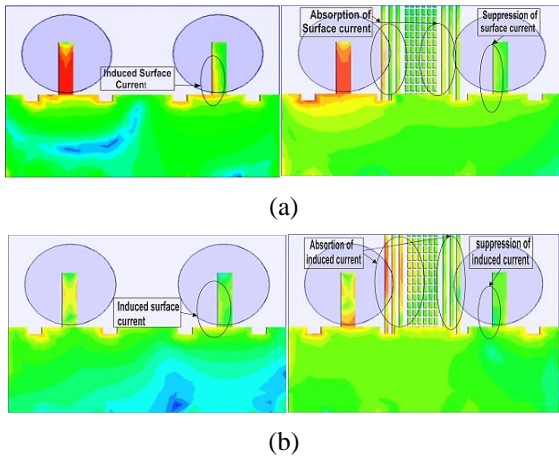


Fig. 6.  $J_{surf}$  current distribution plots at: (a) 5.6 GHz and (b) 8.05 GHz.

#### C. MIMO performance parameters

The diversity performance of a MIMO system is judged by its performance parameters. In this regard, the envelope correlation coefficient (ECC) and total active

reflection coefficient (TARC) have been measured for the proposed MIMO DRA system. A maximum threshold of  $ECC < 0.5$ ,  $TARC < 0$  dB is allowed for an acceptable MIMO system [8]. The proposed design has  $ECC < 0.001$  and  $TARC < -20$  dB, in both bands, as shown in Fig. 7 which assures the optimum performance of the suggested MIMO antenna. Simulated and measured radiation patterns for  $E$ -planes and  $H$ -planes are shown in Fig. 7 (c). The fabrication and measurements imperfections cause slight distortion in radiation patterns. The comparison of the proposed work with the reviewed literature is given in Table 1.

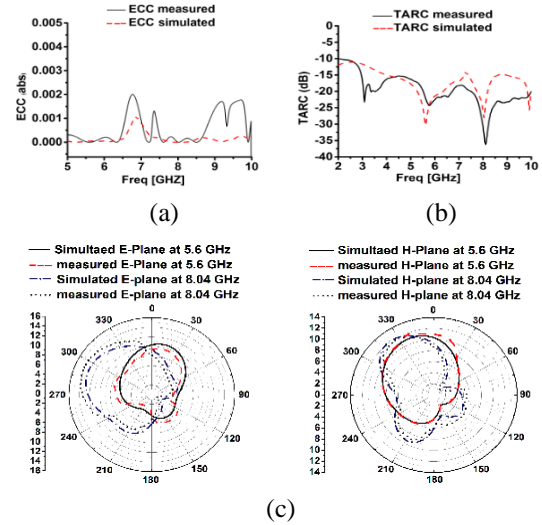


Fig. 7. MIMO performance parameters: (a) ECC, (b) TARC, and (c) radiation patterns.

Table 1: Comparison of the proposed work with the reviewed literature

Ref.	Freq. MHz/GHz	Isolation	Antenna Size [mm <sup>3</sup> ]
[1]	803–823 MHz 2.44–2.9 GHz	20 dB 14 dB	50×100×1.56
[2]	3.4–3.7 GHz 5.1–5.35 GHz	13 dB 16 dB	50 ×50×1.6
[3]	2.4 GHz 5.2 GHz	20 dB 18 dB	40×80×1
[7]	5.15–5.35 GHz	35 dB	60×60×1
This work	5.5–5.8 GHz 8–8.1 GHz	28 dB 41 dB	28×38×1.6

### V. CONCLUSION

A dual-port dual-band MIMO DRA for high gain WLAN and X-band application is proposed. The design is fabricated on a 1.6 mm thick FR-4 substrate. A via-less EBG structure is employed to achieve effective isolation between antenna elements. The measured results demonstrate the isolation better than 20 dB in both bands. MIMO performance criteria such as ECC,

TARC and radiation patterns also exhibit excellent performance. The proposed design exhibits excellent impedance match and isolation, without compromising the compactness. The total antenna is  $0.72 \lambda_0 \times 0.52 \lambda_0$  in size at the lower frequency band.

## REFERENCES

- [1] M. S. Sharawi, A. B. Numan, M. U. Khan, and D. N. Aloï, "A dual-element dual-band MIMO antenna system with enhanced isolation for mobile terminals," *IEEE Antennas and Wireless Propagation Letters*, vol. 11, pp. 1006-1009, 2012.
- [2] A. A. Khan, M. H. Jamaluddin, S. Aqeel, J. Nasir, J. U. R. Kazim, and O. Owais, "Dual-band MIMO dielectric resonator antenna for WiMAX/WLAN applications," *IET Microwaves, Antennas & Propagation*, vol. 11, no. 1, pp. 113-120, 2017.
- [3] J. Kim, M. Han, C. Lee, and J. Choi, "Dual band MIMO antenna using a decoupling network for WLAN application," *13th International Conference on Advanced Communication Technology (ICACT2011)*, Seoul, pp. 624-627, 2011.
- [4] M. T. Islam and M. S. Alam, "Compact EBG structure for alleviating mutual coupling between patch antenna array elements," *Progress In Electromagnetics Research*, vol. 137, pp. 425-438, 2013.
- [5] D. Guha, S. Biswas, T. Joseph, and M. T. Sebastian, "Defected ground structure to reduce mutual coupling between cylindrical dielectric resonator antennas," *Electronics Letters*, vol. 44, no. 14, pp. 836-837, 2008.
- [6] S. H. Zainud-Deen, H. A. Malhat, and K. H. Awadalla, "Reduction of mutual coupling between two dielectric resonator antennas mounted on a circular cylindrical ground plane," *IEEE Antennas and Propagation Society International Symposium (APSURSI)*, pp. 1-4, 2010.
- [7] X. M. Wang, Z. B. Weng, Y. C. Jiao, Z. Zhang, and F. S. Zhang, "Dual-polarized dielectric resonator antenna with high isolation using hybrid feeding mechanism for WLAN applications," *Progress In Electromagnetics Research Letters*, vol. 18, pp. 195-203, 2010.
- [8] S. H. Chae, S. K. Oh, and S. O. Park, "Analysis of mutual coupling, correlations, and TARC in WiBro MIMO array antenna," *IEEE Antennas Wireless Propag. Lett.*, vol. 6, pp. 122-125, 2007.
- [9] R. K. Mongia and P. Bhartia, "Dielectric resonator antennas—A review and general design relations for resonant frequency and bandwidth," *International Journal of Microwave and Millimeter-Wave Computer-Aided Engineering*, vol. 4, no. 3, pp. 230-247.



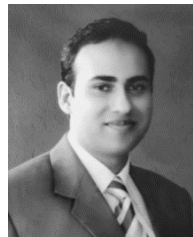
**Muhammad Zia Hameed** received B.Sc. Electronics Engineering in 2012 from The Islamia University of Bahawalpur, Punjab Pakistan. He is currently working as a Research Associate at University of Engineering and Technology (UET), Taxila. Recently he is awarded a funded M.S. studentship by UET Taxila. His main research interests are in DRAs, metamaterials and high gain antennas.



**Shabbir Majeed Chaudhry** received B.Sc. in Electrical Engineering and M.Sc. Electrical Engineering in 2000 and 2003, from University of Engineering and Technology, (UET) Taxila, Pakistan. He also received his Ph.D. degree in Electrical Engineering from UET Taxila and since 2006 onwards, he is working as an Assistant Professor in the same University.



**Rashid Saleem** received B.S. Electronic Engineering from G.I.K Institute of Engineering Sciences and Technology, Pakistan, in 1999. He received M.S. from UET Taxila through Center for Advanced Studies in Engineering, Pakistan, in 2006 and Ph.D. from the University of Manchester, United Kingdom in 2011. Currently, he is working as Assistant Professor at University of Engineering and Technology (UET), Taxila, Pakistan.



**Muhammad Farhan Shafique** received the B.Eng. degree from Hamdard University, Karachi, Pakistan, in 2003, M.S. degree from the University of Paris East Marne-La-Vallée, Paris, France, in 2005 and Ph.D. in Electronic and Communications Engineering from The University of Leeds, UK in 2010. He is working as an Associate Director at Center for Advanced Studies in Telecommunications (CAST).



**Sabih ur Rehman** is working as a Lecturer at Charles Sturt University, Australia. Sabih has completed his Ph.D. in the area of vehicular ad-hoc networks. Sabih's research expertise lie in the areas of Wireless Propagation and Antenna Modeling.