

Gain Enhancement of a Traditional Horn Antenna using 3D Printed Square-Shaped Multi-layer Dielectric Lens for X-band Applications

Aysu Belen¹, Peyman Mahouti^{*2}, Filiz Güneş³, and Özlem Tari⁴

¹Hybrid and Electric Vehicles Technology, Iskenderun Vocational School of Higher Education
Iskenderun Technical University, Hatay, TURKEY
aysu.belen@iste.edu.tr

²Department of Electronic and Automation, Istanbul University-Cerrahpaşa, Istanbul/TURKEY
pmahouti@iuc.edu.tr

³Department of Electronics and Communication, University of Yıldız Technical, İstanbul, TURKEY
gunes@yildiz.edu.tr

⁴Department of Mathematics and Computer Science, Istanbul Arel University, Büyükçekmece, Istanbul-TURKEY
ozlemilgin@arel.edu.tr

Abstract — In this work, gain of a traditional horn antenna is enhanced up to 2.9 dB over X-band using 3D printed square-shaped multi-layer lens. For this purpose, firstly the multi-layer lenses are designed using Invasive Weed Optimization (IWO) and simulated in 3-D CST Microwave Studio (MWS) environment as consisting of square-shaped five layers with variable dielectric constants and heights. Thus, optimum values of the dielectric constants and heights are resulted limiting from 1.15 to 2.1 and 9.2 mm to 10 mm, respectively compatible for Fused Deposition Modeling (FDM) based 3D-printing process. Finally, the optimum lens is realized by 3D printer via FDM evaluating infill rate of cheap Polylactic Acid (PLA) material for each layer. The simulated and measured performance of the multi-layer dielectric structures are hand to hand. The horn antenna equipped by our proposed dielectric lens achieves gain enhancement of the traditional antenna up to 2.9 dB over the operation band. Furthermore, the proposed design is compared with the counterpart designs in literature and based on the comparison results it can be said that the proposed design achieves the better performance in the smaller in size as equipped a traditional X-band horn antenna.

Index Terms — 3D printer, dielectric lens, fused deposition modeling, gain enhancement.

I. INTRODUCTION

The X-band is the designation for a band of frequencies. In radar engineering, the frequency range is specified by the Institute of Electrical and Electronics Engineers (IEEE) at 8.0–12.0 GHz. X-band have a wide

range of applications of civil, military, weather monitoring, air traffic control, maritime vessel traffic control, defense tracking, and vehicle speed detection etc. each of the mentioned applications requires high performance sub-system stages such as bandpass filter [1], microwave absorber [2], high isolated MIMO Array [3], which are a thought-provoking topic for microwave engineers.

One of the most important elements in wireless communication systems is antenna with high gain characteristics. Although antenna arrays are a common solution since gain increase can be obtained with the increase of array element alongside high level of loss in feeding network which causes decrease in efficient, complexity of design. Another solution for high gain performance is usage of dielectric lens structures. Dielectric lens have been used for gain enhancements of microwave antennas due to their ability of focusing the incoming electromagnetic waves. Also, the dielectric lens antenna has advantages of low loss and wide operation band. These designs have been used in many applications such as millimeter wave, automotive radar, satellite or indoor communication applications [4-11], or are used to beam forming for generation of multiple beams [12-13]. However, widespread dielectric lenses like Luneburg, Einstein, dielectric rod, Fresnel lens are commonly optical or quasi-optical devices, which have 3D design structures that make them hard to fabricate with dielectric materials. However, with the advances in 3D printing technology, applications of these devices are increasing.

One of the most recent applications of 3D printing technology is prototyping of microwave designs such as

antennas [14-16]. Due to their high accurate, fast printing ability even for the most complex structures whose prototyping by traditional methods becomes either impractical or costly, the interest to usage of 3D printing technology for microwave design prototyping become widespread [17-23].

Herein, it is aimed at designing and realizing a square shaped multi-layer lens for gain enhancement of a X-band traditional horn antenna using 3D printing technology. For this purpose, in the next section, firstly design procedure of the proposed multi-layer lens structure will be presented alongside of its simulated results. Then in Section 3, the antenna design will be prototyped via the use of 3D printing technology and its experimental results are compared with its simulated results and performance results of the counterpart designs in literature. Finally, the paper will end conclusion.

II. DESIGN AND SIMULATION

Horn antenna is one of the most commonly used antenna types in wireless communication systems such as astronomy, satellite tracking and high power RF systems [24]. Although they have a relatively good gain characteristics, they are limited by their dimension limitation where they should have a certain size with respect to their operation frequencies wavelengths, otherwise they would have efficiency problems. For the last decades many methods have been presented for performance improvement of horn antennas. Commonly hybrid designs had been presented to improve performance measures such as side lobe level, cross polarization [25-26], Corrugated horns [27-29], dielectric core horns [30], and strip-loaded horns [31] are the typical examples. Placement of dielectric lens structures to the aperture of antenna designs is one of the commonly used methods for performance improvement, where by placing the carefully selected materials and geometrical designs [32-35].

Herein, a squared shaped multi-layer dielectric lens (Fig. 1) is proposed as consisting of layers having variable heights and dielectric constants. In the design it should be noted that (i) the gain may be increased/decreased by increasing/decreasing the dielectric width of the square layers; (ii) Operation frequency can be shifted via the width of layers; (iii) the dielectric constant of the lens material is also an important design parameter for focusing the EM waves [35-36].

In Table 1, geometrical values of the proposed designs are given. These values have been obtained by using a novel meta-heuristic optimization algorithm Invasive Weed Optimization (IWO). IWO is a population-based method inspired from the behavior of weed colonies that they search for an optimal environment to live [37]. IWO had shown great potential in application of; aperiodic planar thinned array antennas [38], the Shape of Non-Planar Electronically Scanned Arrays

[39], directivity maximization of Uniform Linear Array of Half-wavelength Dipoles [40], Low Pass Elliptic Filter [41], Reflector Antenna [42] and design of a compact step impedance transmission line low pass filter [43]. Here similar to [44], an IWO algorithm coded in MATLAB environment has been used alongside of CST 3D EM simulator to obtain optimal performance criteria's based on the following cost function:

$$\text{Cost} = \sum_{f_{\min}}^{f_{\max}} \frac{C_1}{D_i(f)} + \frac{C_2}{|S_{11}(f)|}, \quad (1)$$

where C values have been found as $C_1=0.9$, $C_2=0.3$ by trial and error [44]. Here the goal is to maximize both of the performance measures within the given operation band between $f_{\min}=8$ GHz and $f_{\max}=12$ GHz. Thus, both S_{11} and directivity D are optimized along the X-band using the cost function given by (1). In Fig. 2, a flow chart of the proposed design optimization process is presented.

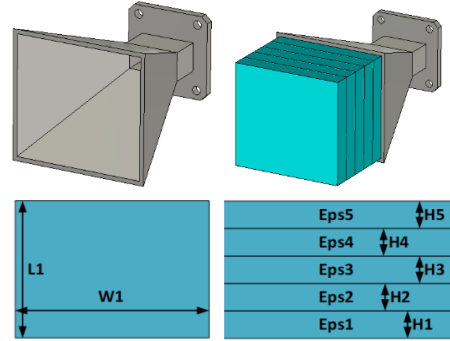


Fig. 1. Schematics of the proposed multi-layer squared lens antenna.

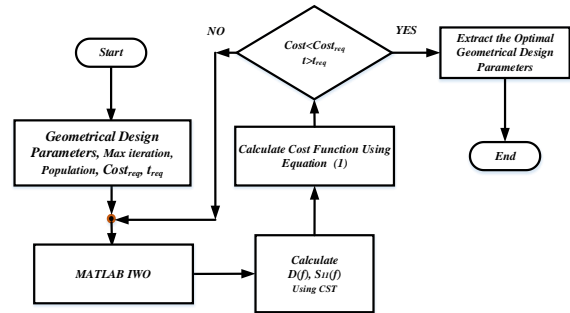


Fig. 2. Flow chart of the SIW antenna design optimization.

Table 1: Optimally selected design values

Eps1	1.66	H1	9.2 mm
Eps2	1.45	H2	10 mm
Eps3	1.15	H3	9.8 mm
Eps4	1.38	H4	9.9 mm
Eps5	2.1	H5	10 mm
L1	60mm	W1	60mm

In Fig. 3, the simulated performance of horn antenna with and without the multi-layer dielectric lens structure are presented. As it can be seen from the Fig. 2, not only the proposed design improves the overall radiation performance of the horn antenna over the operation band but also it has a low level of deteriorating on the performance of the return loss. A more detailed performance comparison of both antenna designs are presented in Table 2, where it can be clearly seen that the proposed dielectric lens antenna improves the realized gain characteristics up to 2.9dB over the aimed operation frequency.

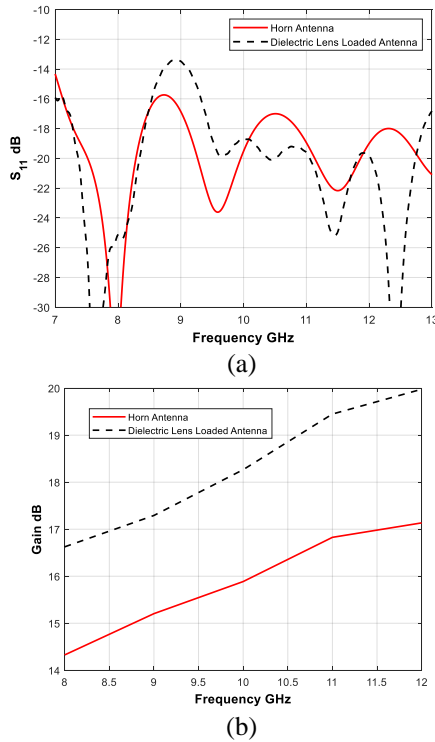


Fig. 3. Simulated (a) return loss and (b) gain of horn antenna with and without dielectric lens structure.

Table 2: Simulated performances of horn/horn antenna equipped with multi-layer dielectric lens

f (GHz)	Realized Gain (dB)	Enhanced (dB)	3dB (Angle)	Side lobe level (dB)
8	14.4 / 16.6	2.2	32.1 / 25.5	-15.2 / -16.3
9	15.2 / 17.3	2.1	27.9 / 21.2	-12.5 / -12.6
10	15.9 / 18.3	2.4	26.4 / 19.7	-12.7 / -16.6
11	16.9 / 19.4	2.5	22.4 / 17.6	-11.3 / -14.7
12	17.1 / 20	2.9	22.3 / 16.6	-10.8 / -15.2

III. EXPERIMENT RESULTS

3D printing technology is one of the recent innovation that is being used for fast, accurate and low cost manufacturing of microwave devices [45]. Recently 3D printing technology has been applied for manufacturing

of Multi-layered Cylindrical Dielectric Lens Antenna [36], Non-Uniform Reflectarrays [45], Quasi Yagi Antenna for indoor application [14], or prototyping of Horn Antennas for X-band applications [15], Electrically Small Spherical Wire Antennas [46].

In this section, the proposed multi-layer lens antenna has been prototyped via the use of a commercial 3D printer, CEL Robox® Micro manufacturing platform [47]. The 3D printer uses PLA material “PLA Filament - Polar White RBX-PLA-WH002” [48]. Thanks to the unique ability of 3D printer’s infill rate adjustment, not only it allows to the lower weight of the designs but also it is possible to create dielectric materials with variable dielectric constant values [49-50]. Some cases of the PLA material with the different dielectric constants are presented in Table 3. The analytical expression in Eq. (2) between infill rate and dielectric constant is obtained via regression method using the experimental data given in Table 3:

$$\epsilon_r = -1.3 \times 10^{-6} x^3 + 0.0374x + \frac{6.42}{x} + 0.217, \quad (2)$$

where, x indicates the infill rate in %.

Table 3: Dielectric constant value of PLA with respect to the variant infill rate [49]

Infill Rate %	Dielectric Constant ϵ_r	Loss Tangent
18	1.24	0.002
33	1.6	0.004
73	2.53	0.006
100	2.72	0.008

The 3D printed multi-layer dielectric antenna and its measurement setup are presented in Fig. 4. A network analyzer with a measurement bandwidth of 9 KHz - 13.5GHz and a horn antenna [51] is used for the measuring the experimental results of the antenna.



Fig. 4. 3D printed antenna design.

The measured S_{11} , and radiation patterns of the 3D printed multi-layer dielectric lens antenna are given in Figs. 5-6 and Table 4. As it can be seen from Fig. 5, similar to the simulated results, placement of the 3D lens structure to the aperture of the antenna does not have any concerning distortive effect on the return loss performance. The design achieves a return loss characteristics of less than -10 dB over the operation band of 8-12 GHz. The measured radiation patterns of the proposed antenna with and without lens structure are

presented in Fig. 6, and Table 4. From the measurement results it can be concluded that, just it was expected from the simulated results, the 3D printed lens structure increases the radiation performance of the antenna design 2.9 dB over the operation band of 8-12 GHz.

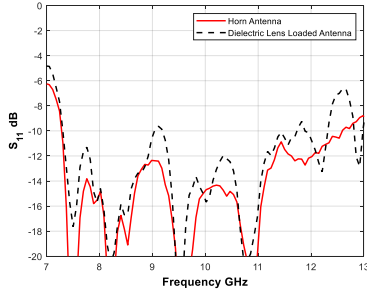


Fig. 5. Measured return loss.

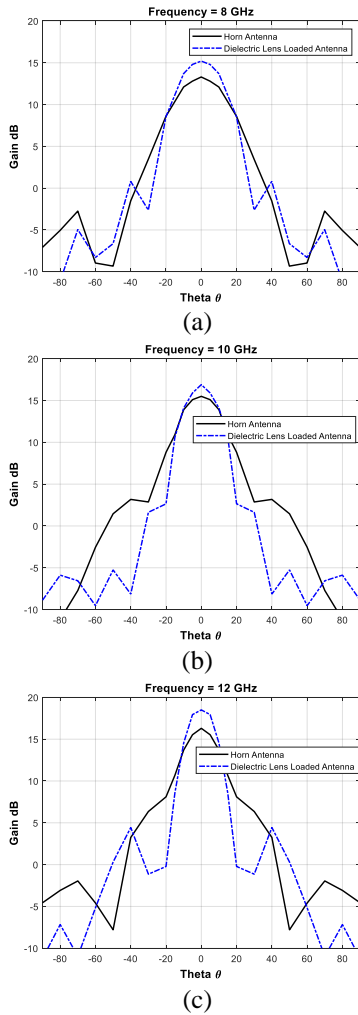


Fig. 6. Measured radiation patterns of the prototyped antenna at: (a) 8 GHz, (b) 10 GHz, and (c) 12 GHz.

Table 4: Maximum gain (dB) comparison between simulation and measurement

Frequency (GHz)	Simulated	Measured
8	16.2	15.2
9	17.3	16.4
10	18.3	16.9
11	19.5	18.1
12	19.9	18.6

Table 5: Comparison of gain (dB) of typical dielectric loaded antenna modules

	Size (mm)	Operation Band (GHz)				
		8	9	10	11	12
Here	68x65x149	15.2	16.5	16.9	18.1	18.5
[52]	279x244x159	16	18	14.8	17	15
[53]	85.1x30.8x15.9	8.5	9	9	9	10
[54]	90.7x210x210	---	---	17	---	---
[55]	87.4x59.3x80	14	15.5	16.5	15	17

Furthermore a comparison of gain (dB) performance of the horn antenna equipped with multi-layer dielectric lens antenna with the counterpart designs in literature [42-55] has been presented in Table 5. From the comparisons, it can be concluded that the proposed dielectric lens structure can be used to model a high performance antenna that achieves better gain vs. size performance within the requested operation frequency compared to its counterpart designs.

VI. CONCLUSION

In this work, design and realization of a squared shaped multi-layer dielectric lens antenna via the use of 3D printing technology has been achieved. By using the unique features of 3D printing technology a dielectric lens structures with multiple layers that each has different values of substrate height and dielectric constant values are prototyped. By placing the proposed multi-layer dielectric lens stricter to the aperture of a traditionally horn antenna the gain performance of the antenna has been enhanced without deteriorating the return loss characteristics of the antenna over the selected operation up to 2.9dBi. Furthermore the experimental results of the prototyped antenna is compared with the counterpart dielectric loaded lens antenna designs in literature and found to be a better solution both in means of size and gain enhancement performance for the selected operation band.

ACKNOWLEDGMENT

We would like to express our special thanks of gratitude to the Research Fund of the Yıldız Technical University for founding our research under project number of FAP-2018-3427, TÜBİTAK 2211/A, YÖK 100/2000, microwave and antenna laboratories of Yıldız

Technical University, and Aktif Nesor Elektronik for providing their support for our researches.

REFERENCES

- [1] B. Zheng, S. Wong, Y. Wu, and Q. Chu, "A novel stack PCB structure for X-band cavity bandpass filter implementation," *2017 International Applied Computational Electromagnetics Society Symposium (ACES)*, Suzhou, pp. 1-2, 2017.
- [2] S. Vinayasree, M. A. Soloman, V. Sunny, P. Mohanan, P. Kurian, and M. R. Anantharaman, "A microwave absorber based on strontium ferrite-carbon black-nitrile rubber for S and X-band applications," *Composites Science and Technology*, vol. 82, pp. 69-75, 2013.
- [3] J. Jiang, Y. Xia, and Y. Li, "High isolated X-band MIMO array using novel wheel-like metamaterial decoupling structure," *Applied Computational Electromagnetics Society Journal*, vol. 34, no. 12, 2019.
- [4] J. R. Risser, *Microwave Antenna Theory and Design*. New York, NY, USA: McGraw-Hill, 1949.
- [5] B. Chantraine-Bares, R. Sauleau, L. L. Coq, and K. Mahdjoubi, "A new accurate design method for millimeter-wave homogeneous dielectric substrate lens antennas of arbitrary shape," *IEEE Trans. Antennas Propag.*, vol. 53, no. 3, pp. 1069-1082, Mar. 2005.
- [6] W. E. Kock, "Metallic delay lens," *Bell System Tech. J.*, vol. 27, pp. 58-82, Jan. 1948.
- [7] W. E. Kock, "Metal lens antennas," *Proc. IRC*, vol. 34, no. 11, pp. 826-836, Nov. 1946.
- [8] B. Schoenlinner, X. Wu, J. P. Ebling, G. V. Eleftheriades, and G. M. Rebeiz, "Wide-scan spherical-lens antennas for automotive radars," *IEEE Trans. Microwave Theory Tech.*, vol. 50, pp. 2166-2175, 2002.
- [9] B. Fuchs, O. Lafond, S. Rondineau, M. Himdi, and L. Le Coq, "Off-axis performances of half Maxwell fish-eye lens antennas at 77GHz," *IEEE Trans. Antennas Propag.*, vol. 55, pp. 479-482, 2007.
- [10] J. R. Costa, C. A. Fernandes, G. Godi, R. Sauleau, L. Le Coq, and H. Legay, "Compact Ka-band lens antennas for LEO satellites," *IEEE Trans. Antennas Propag.*, vol. 56, pp. 1251-1258, 2008.
- [11] C. A. Fernandes, "Shaped dielectric lenses for wireless millimeter-wave communications," *IEEE Antennas Propag. Mag.*, vol. 41, pp. 141-150, 1999.
- [12] O. Lafond, M. Caillet, B. Fuchs, S. Palud, M. Himdi, S. Rondineau, and L. Le Coq, "Millimeter wave reconfigurable antenna based on active printed array and inhomogeneous lens," *Eur. Microwave Conf.*, Amsterdam, Holland, pp. 147-150, 2008.
- [13] B. Fuchs, S. Palud, O. Lafond, M. Himdi, and S. Rondineau, "Système antennaire dont le diagramme de rayonnement est reconfigurable parmi des diagrammes de rayonnement sectoriels et directifs, et dispositifs émetteur et/ou récepteur correspondant," *French Patent 0756664*, July 20, 2007.
- [14] M. A. Belen and P. Mahouti, "Design and realization of quasi Yagi antenna for indoor application with 3D printing technology," *Microw. Opt. Technol. Lett.*, vol. 60, no. 9, pp. 2177-2181, 2018. <https://doi.org/10.1002/mop.31319>
- [15] P. Mahouti, F. Güneş, M. A. Belen, and A. Çalışkan, "A novel design of non-uniform reflectarrays with symbolic regression and its realization using 3-D printer," *Applied Computational Electromagnetics Society Journal*, vol. 34, no. 2, 2019.
- [16] J. J. Adams, E. J. Duoss, T. Malkowski, M. Motala, B. Y. Ahn, R. G. Nuzzo, J. T. Bernhard, and J. A. Lewis, "Conformal printing of electrically small antennas on three-dimensional surfaces," *Advanced Materials*, vol. 23, no. 11, pp. 1304-1413, 2011.
- [17] G. Shaker, L. Ho-Seon, S. Safavi-Naeini, and M. Tentzeris, "Printed electronics for next generation wireless devices," *IEEE Antenna and Propagation Conference (LAPC)*, pp. 1-5, Nov. 2011.
- [18] J. Mei, M. Lovell, and M. Mickle, "Formulation and processing of novel conductive solution inks in continuous inkjet printing of 3-D electric circuits," *IEEE Transactions on Electronics Packaging Manufacturing*, vol. 28, no. 3, pp. 265-273, July 2005.
- [19] G. Shaker, S. Safavi-Naeini, N. Sangary, and M. Tentzeris, "Inkjet printing of ultrawideband (UWB) antennas on paper based substrates," *Antennas and Wireless Propagation Letters, IEEE*, vol. 10, pp. 111-114, 2011.
- [20] J. Hester, S. Kim, J. Bito, T. Le, J. Kimionis, D. Revier, C. Saintsing, W. Su, B. Tehrani, A. Traille, B. S. Cook, and M. M. Tentzeris, "Additively manufactured nanotechnology and origami-enabled flexible microwave electronics," *Proc. IEEE*, vol. 103, no. 4, pp. 583-606, pr. 2015.
- [21] J. Kimionis, A. Georgiadis, M. Isakov, H. J. Qi, and M. M. Tentzeris, "3D/inkjet-printed origami antennas for multi-direction RF harvesting," in *IEEE MTT-S Int. Microw. Symp. (IMS)*, Phoenix, AZ, USA, pp. 1-4, May 2015.
- [22] R. Martinez, et al., "Planar monopole antennas on substrates fabricated through an additive manufacturing process," in *9th Eur. Conf. Antennas and Propag. (EuCAP)*, Lisbon, Portugal, Apr. 2015.
- [23] B. Tehrani, B. S. Cook, and M. M. Tentzeris, "Post-process fabrication of multi-layer mm-wave on-package antennas with inkjet printing," in *2015 IEEE Int. Symp. Antennas and Propag. (APSURSI)*, Vancouver, BC, Canada, July 2015.
- [24] F. Karshenas, A. R. Mallahzadeh, and A. Imani,

- “Modified TEM horn antenna for wideband applications,” in *2009 13th International Symposium on Antenna Technology and Applied Electromagnetics and the Canadian Radio Science Meeting, IEEE*, pp. 1-5, Feb. 2009.
- [25] E. Lier and P. S. Kildal, “Soft and hard horn antennas,” *IEEE Trans. Antennas Propag.*, vol. 36, no. 8, pp. 1152-1157, 1988.
- [26] E. Lier, “Review of soft and hard horn antennas, including metamaterial based hybrid-mode horns,” *IEEE Trans. Antennas Propag. Mag.*, vol. 52, no. 2, pp. 31-39, 2010.
- [27] A. J. Simmons and A. F. Kay, “The scalar feed – A high performance feed for large paraboloid reflectors,” in *Design and Construction of Large Steerable Aerials*, vol. 21, pp. 213-217, 1966.
- [28] H. Minnett and B. Thomas, “A method of synthesizing radiation patterns with axial symmetry,” *IEEE Trans. Antennas Propag.*, vol. 14, no. 5, pp. 654-656, 1966.
- [29] V. Rumsey, “Horn antennas with uniform power patterns around their axes,” *IEEE Trans. Antennas Propag.*, vol. 14, no. 5, pp. 656-658, 1966.
- [30] P. J. B. Clarricoats, A.D. Olver, and M. S. A. S. Rizk, “A dielectric loaded conical feed with low cross-polar radiation,” *Proc. URSI Symp. Electromagnetic Theory*, Santiago, Spain, pp. 351-354, Aug. 1983.
- [31] E. Lier and T. Schaug-Pettersen, “The strip-loaded hybrid-mode feed horn,” *IEEE Trans. Antennas Propag.*, vol. 35, no. 9, pp. 1086-1089, 1987.
- [32] M. A. Belen, P. Mahouti, and M. Palandöken, “Design and realization of novel frequency selective surface loaded dielectric resonator antenna via 3D printing technology,” *Microwave and Optical Technology Letters*, vol. 62, no. 5, pp. 2004-2013, 2020.
- [33] M. A. Belen and P. Mahouti, “Design of nonuniform substrate dielectric lens antennas using 3D printing technology,” *Microwave and Optical Technology Letters*, vol. 62, no. 2, pp. 756-762, 2020.
- [34] A. Belen, F. Güneş, P. Mahouti, and M. Palandöken, “A novel design of high performance multi-layered cylindrical dielectric lens antenna using 3D printing technology,” *International Journal of RF and Microwave Computer-Aided Engineering*, vol. 30, no. 1, e21988, 2020.
- [35] M. A. Belen and P. Mahouti, “Realization of dielectric sheets for gain improvement of ultra-wideband horn antennas using 3D printer technology,” *Applied Computational Electromagnetics Society Journal*, vol. 34, no. 5, 2019.
- [36] P. Mahouti, M. A. Belen, F. Güneş, and R. Yurt, “Design and realization of multi-layered cylindrical dielectric lens antenna using 3D printing technology,” *Microwave and Optical Technology Letters*, vol. 61, no. 5, pp. 1400-1403, 2019.
- [37] M. Misaghi and M. Yaghoobi, “Improved invasive weed optimization algorithm (IWO) based on chaos theory for optimal design of PID controller,” *Journal of Computational Design and Engineering*, vol. 6, no. 3, pp. 284-295, 2019.
- [38] S. Karimkashi and A. A. Kishk, “Invasive weed optimization and its features in electromagnetics,” *IEEE Transactions on Antennas and Propagation*, vol. 58, no. 4, pp. 1269-1278, 2010.
- [39] S. Maddio, G. Pelosi, M. Righini, S. Selleri, and I. Vecchi, “Optimization of the shape of non-planar electronically scanned arrays for IFF applications via multi-objective invasive weed optimization algorithm,” *Applied Computational Electromagnetics Society Journal*, 2020.
- [40] A. R. R. Mallahzadeh, H. Oraizi, and Z. Davoodi-Rad, “Application of the invasive weed optimization technique for antenna configurations,” *Progress in Electromagnetics Research*, vol. 79, pp. 137-150, 2008.
- [41] M. Hayati, M. Amiri, and S. H. Sedighy, “Design of compact and wideband suppression low pass elliptic filter by n-segment step impedance transmission line,” *Applied Computational Electromagnetics Society Journal*, vol. 30, no. 5, 2015.
- [42] A. R. Mallahzadeh and P. Taghikhani, “Cosecant squared pattern synthesis for reflector antenna using a stochastic method,” *Applied Computational Electromagnetics Society Journal*, vol. 26, no. 10, pp. 823, 2011.
- [43] H. R. Khakzad, S. H. Sedighy, and M. K. Amirhosseini, “Design of compact SITLs low pass filter by using invasive weed optimization (IWO) technique,” *Applied Computational Electromagnetics Society Journal*, vol. 28, no. 3, pp. 228-233, 2013.
- [44] A. Belen, F. Güneş, and P. Mahouti, “Design optimization of a dual-band microstrip SIW antenna using differential evolutionary algorithm for X and K-band radar applications,” 2020.
- [45] A. Belen, F. Güneş, M. A. Belen, and P. Mahouti, “3D printed wideband flat gain multi-layer nonuniform reflectarray antenna for X-band applications,” *International Journal of Numerical Modelling: Electronic Networks, Devices and Fields*, e2753, 2020.
- [46] O. S. Kim, “Rapid prototyping of electrically small spherical wire antennas,” *Antennas and Propagation, IEEE Transactions*, vol. 62, no. 7, pp. 3839-3842, 2014.
- [47] Available on 19.6.2018. <http://cel-uk.com/3d-printer/rbx01-480.html>
- [48] Available on 21.11.2018. <http://cel-uk.com/3d-printer/filament/pla/rbx-pla-wh002.html>
- [49] S. Zhang, C. C. Njoku, W. G. Whittow, and J. C.

Vardaxoglou, "Novel 3D printed synthetic dielectric substrates," *Microw. Opt. Technol. Lett.*, vol. 57, pp. 2344-2346, 2015. doi:10.1002/mop.29324.

- [50] P. Mahouti, "Boyutlu Yazıcı Teknolojisi ile Bir Mikroşerit Yama Antenin Maliyet Etkin Üretimi," *Journal of Engineering Sciences and Design*, Kabul Edildi, 2019. (in Turkish).
- [51] LB8180, "0.8-18 GHz broadband horn antenna," Aug. 14 2017. Available at: http://www.ainfoinc.com/en/p_ant_h_brd.asp
- [52] A. S. Türk, A. K. Keskin, and M. D. Şentürk, "Dielectric loaded TEM horn-fed ridged horn antenna design for ultrawideband ground-Penetrating impulse radar," *Turkish J. Elec. Eng. & Comp. Sci.*, vol. 23, pp. 1479-1488, 2015.
- [53] R. J. Bauerle, R. Schrimpf, E. Gyorko, and J. Henderson, "The use of a dielectric lens to improve the efficiency of a dual-polarized quad-ridge horn from 5 to 15 GHz," *IEEE Transactions on Antennas and Propagation*, vol. 57, no. 6, June 2009.
- [54] J. Tak, D.-G. Kang, and J. Choi, "A lightweight waveguide horn antenna made via 3d printing and conductive spray coating," *Microwave and Optical Technology Letters*, vol. 59, no. 3, Mar. 2017.
- [55] M. F. Ain, A. Othman, and Z. A. Ahmad, "Hybrid dielectric resonator integrated pyramidal horn antenna," *Microwave and Optical Technology Letters*, vol. 55, no. 6, June 2013.



Aysu Belen received her Ph.D. degree in Electronics and Communication Engineering from the Yıldız Technical University in 2021. Currently, she is a Lecturer in İskenderun Technical University. Her main research areas are optimization of microwave circuits, device modeling, and computer aided circuit design and microwave amplifiers.



Peyman Mahouti received his M.Sc. and Ph.D. degree in Electronics and Communication Engineering from the Yıldız Technical University, Turkey, in 2013 and 2016, respectively. He is currently an Associated Professor with the Department of Electronic and Communication, Istanbul University - Cerrahpasa, Turkey. The main research areas are analytical and numerical modelling of microwave devices, optimization techniques for microwave stages, and application of artificial intelligence-based algorithms. His research interests include analytical and numerical modelling of microwave and antenna structures, surrogate-based optimization, and application of artificial intelligence algorithms.



Filiz Güneş received her M.Sc. degree in Electronics and Communication Engineering from the Istanbul Technical University. She attained her Ph.D. degree in Communication Engineering from the Bradford University in 1979. Her current research interests are in the areas of multivariable network theory, device modeling, computer-aided microwave circuit design, monolithic microwave integrated circuits, and antenna designs.



Özlem Tari received her B.Sc., M.Sc. and Ph.D. in Physics Engineering from the Istanbul Technical University (ITU). She was the recipient of the Universidad Carlos III de Madrid Research Fellowship award before accepting her position at Istanbul Arel University in 2010. Her research areas are the phase transitions and phase diagram of some physical systems, Multi-Objective Optimization problems and development of Meta-Heuristic Optimization Algorithms.