

A Band Stop to Band Pass Filter Transformation Utilizing 3-D Printing Technique for C-band Applications

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Abstract – In this paper, a band-pass filter (BPF) based on split-ring resonator (SRR) using a 3-D printing technique for C-band applications is introduced. The proposed filter is designed to operate at a frequency of 3.9 GHz. An innovative technique for printing the substrate with a size of $24 \times 24 \times 1.1$ mm³ using PLA dielectric material is implemented. The copper sheet with a thickness of 0.1 mm is printed on the upper and lower faces of the substrate. First, the SRR band stop filter (BSF) is introduced then two L-Stubbs are inserted to implement an additional band stop region, and this rejoin is adjusted to obtain a band-pass region between the two stopbands. The BPF is operated at a 3-dB bandwidth extended from 3.5 GHz to 4.3 GHz with an S_{21} level of -0.2 dB for the simulated results while it achieves a 3-dB bandwidth within 3.6 GHz to 4.2 GHz (15.3 %) with an S_{21} level of -1.8 dB for the measured results.

Index Terms – 3-D printing, bandpass filter, C-band applications, PLA.

I. INTRODUCTION

Filters play a very important role in many RF microwave applications. They are commonly utilized in transceiver circuits to isolate or merge various frequencies. A band-pass filter allows components to pass in a specific frequency band, known as the passband while blocking other components of frequencies that are higher than or lower than this band [1, 2]. Bandpass filters are commonly used in wireless transmission and reception. The main purpose of the filter is to pass an output signal with a certain range of frequencies allocated for transmission to avoid interference with the neigh-

boring [3, 4]. Several studies are conducted to achieve a bandpass behavior that fulfills modern technological market needs such as compact size, sharp roll-off rate, wide stopband, and low passband insertion loss [5–9]. Various techniques are carried out to achieve the required bandpass behavior as in [10–17]. In [10], the defected ground structure is used to obtain a wide band stop behavior while passing all frequencies in the range of 2.4–14.3 GHz. The stepped impedance resonator (SIR) is one of the most commonly used techniques to provide a bandpass behavior and it succeeded to achieve a triple band (1.85 GHz, 2.575 GHz, and 3.05 GHz) with skew-symmetric (0-degree) tapped-feed structure as in [11]. The open-loop resonator (OLR) technique was carried out in [12] for dual passbands (WLAN and WiMAX). Another technique substrate integrated wave (SIW) was used in [13] to achieve a band-pass response (15.6–32.1 GHz) in the RF and millimetric wave frequency range with an enhanced insertion loss in the passband (> -0.8 dB). To obtain a millimeter band-pass response, a split ring resonator (SRR) was used [14], and the achieved performance was quite enough to make the suggested filter a good candidate for 5G networks.

Nowadays, 3-D printing, or additive manufacturing (AM), is the building block of a three-dimensional object from a digital 3-D model. The entire 3D printing technology can be divided into 3 steps 1st 3D design, 2nd slicing, 3rd 3D printing [15]. 3D printing techniques are used recently in designing microwave components such as filters and antennas. It can be used to construct antenna models for multiband applications as in [16–19]. Additionally, there are various designs of microwave filters based on 3D printing in the RF frequency range

[20–21], and the implemented BPF in [22] was operated in the E-band (60–90 GHz) of the millimetric wave frequency range, but with inconsistent simulation and experimental results due to fabrication tolerance.

II. SRR BSF

The 2-D structure of the SRR BSF is illustrated in Fig. 1. The BSF has a $\lambda/2$ open-loop transmission line and the SRR is fed by a 50Ω microstrip line connected with SMA connectors. The PLA substrate material with a dielectric constant of 3.1, loss tangent of 0.001, and height of 1.1 mm is utilized. The detailed dimensions of the filter parameter are depicted in Fig. 1 (a) and listed in the figure caption. The simulated (CST & HFSS) outcomes of the BSF are illustrated in Fig. 2. The suggested BSF is operating at 5 GHz with 2.7 GHz 3-dB bandwidth from 3.7 GHz to 6.4 GHz and the achieved return loss over the entire stopband is approximately 0.2 dB. To verify the achieved results in Fig. 2 the electric field distribution is simulated at different frequencies outside (3 and 7 GHz) and inside the stopband (5 GHz) as shown in Fig. 3. It is clear that at 3 GHz, the electric field is conducted to port 2 through the open-ended loop as shown in Fig. 3 (a) and the same behavior is noticed when the filter is excited at 7 GHz but the major concentration of field was through the aligned arm of the resonator with the two feedlines as shown in Fig. 3 (c). However, at 5 GHz as shown in Fig. 3 (b), the electric field couldn't pass to port 2 and is concentrated on port 1 and the left part of SRR confirming the capability of the suggested filter to behave as a BSF in the desired band. Furthermore, the current distribution of the suggested filter is demonstrated in Fig. 4 and the current distribution is carried out at the same three frequencies which were used in the field distribution confirming the ability of the suggested filter to pass all frequencies except the desired band from 3.7 to 6.4 GHz.

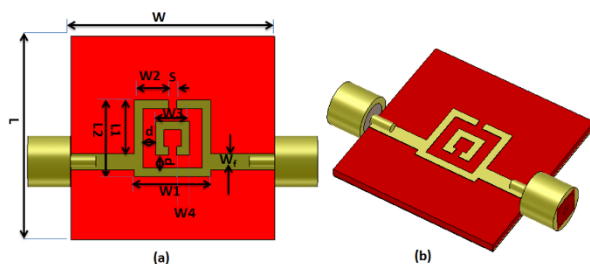


Fig. 1. The configuration of SRR BSF. (a) 2-D configuration with $W = L = 24$ mm, $W_1 = 9$ mm, $W_f = 1.95$ mm, $d = 1.5$ mm, $S = 1$ mm, $W_2 = 4$ mm, $L_1 = 6.3$ mm, $L_2 = 9$ mm, $W_3 = 4$ mm, and $W_4 = 1.5$ mm. (b) 3-D configuration.

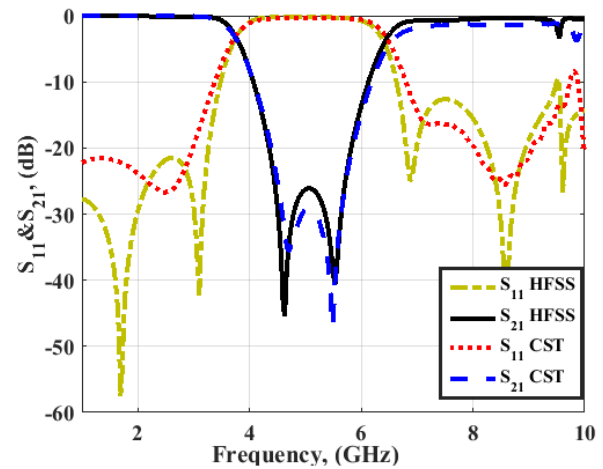


Fig. 2. The simulated SRR BSF S-parameters results.

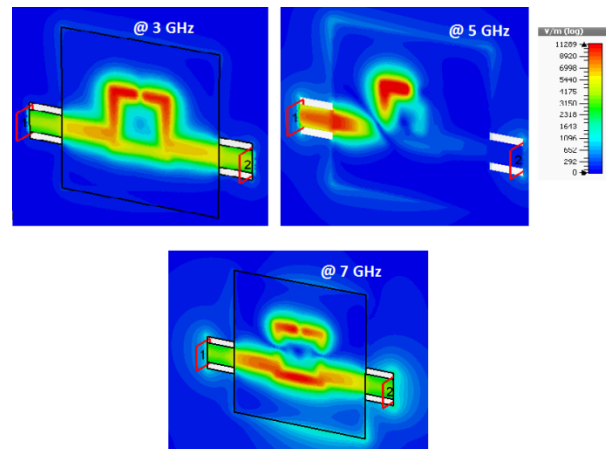


Fig. 3. The simulated distributions of electric field results of SRR BSF at $z=0.6$ mm (inside substrate).

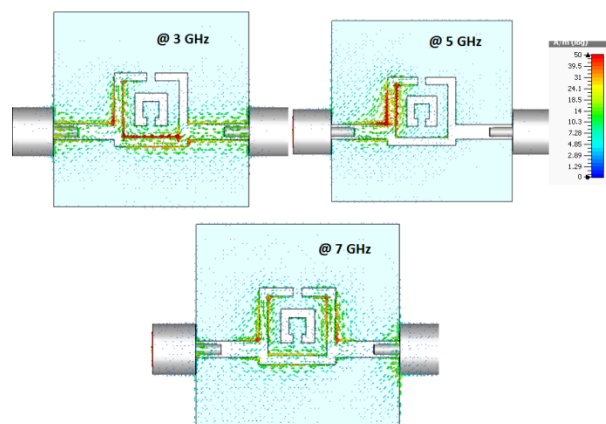


Fig. 4. The current distribution's simulated results of SRR BSF.

III. PROPOSED SRR BPF/BSF

To produce the dual-band operation of the SRR-BSF, an additional resonator is introduced in Fig. 5 with dimensions L_s and W_s . It is worth noting that the dimensions of the additional resonator are larger than the fundamental one, so the achieved rejection band will be in the lower frequency range. Consequently, it is evident from Fig. 6 of the achieved simulated results of insertion and return loss using HFSS and CST programs that the suggested filter has two operating stopbands, the first one covers the range from 2.1 to 3.4 GHz with a deeper insertion loss of 47 dB at 3 GHz, and the second band covers the old frequency range with a reduction of 0.4 GHz (4.4 – 6.4 GHz) and this is due to the coupling with the additional SRR. Furthermore, a new BPF behavior is accomplished in the frequency range (3.5 – 4.3 GHz) with an insertion loss of level 0.2 dB confirming the readability of the suggested BPF to be embedded in different applications that cover the achieved frequency band. There is a discrepancy between HFSS and CST results, especially at the extremely lower and higher frequencies of the achieved rejection bands and this may be due to the different meshing operations of both programs.

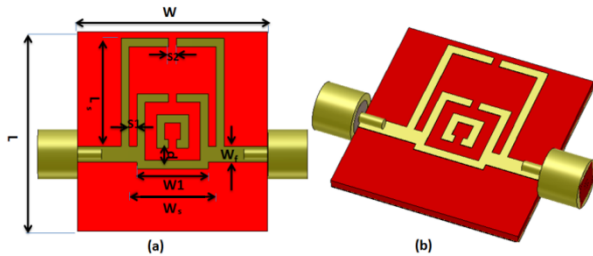


Fig. 5. The configuration of the proposed SRR BPF/BSF (a) 2-D configuration with $W=L=24$ mm, $W_1= 9$ mm, $W_f = 1.95$ mm, $d= 1.5$ mm, $S_1=1$ mm, $S_2= 1$ mm, $L_s= 13$ mm, $W_s = 10$ mm (b) 3-D configuration.

The parametric study is carried out to illustrate the effect of the SRR length (L_s), its width (W_1), and the spacing between inner and outer SRRs (S_1) on the filter performance. The effect of changing the length of L_s on the behavior of the proposed filter is presented in Fig. 7 and it is obvious that the length change has a significant effect on the lower band since the operating frequency is translated to the lower range by increasing L_s , also it has a minor effect on the achieved upper-frequency band. Another parameter is changed to investigate its effectiveness which is the width “ W_1 ”. It can be observed from Fig. 8 that both stopbands are translated to a lower range by increasing W_1 and the level of translation in the higher band is greater than that of the lower band since the shift in the upper band is about 0.8 GHz and the lower band 0.4 GHz when increasing W_1 to 10 mm. Addition-

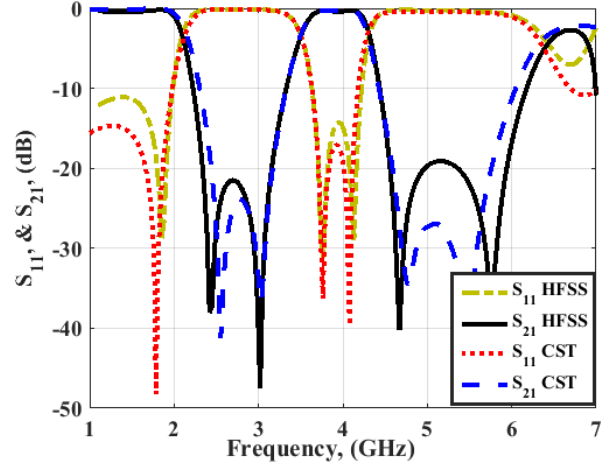


Fig. 6. S-parameters simulated results of SRR BPF/BSF.

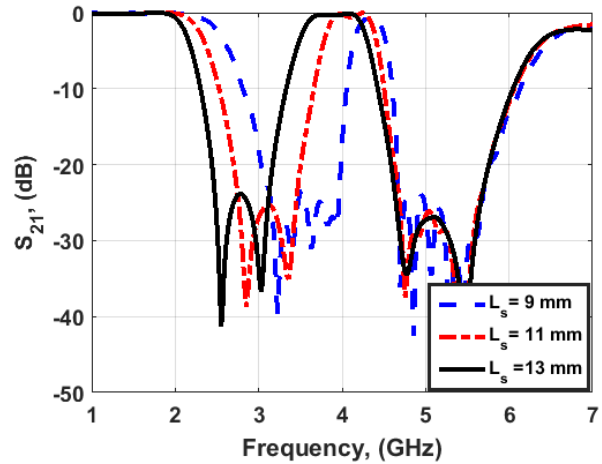


Fig. 7. The S_{21} simulated results of SRR BPF/BSF at different values (L_s).

ally, when increasing W_1 to 11 mm, the upper band is shifted down by 0.6 GHz and the lower band by 0.1 GHz. Consequently, the parameter W_1 has a great influence, especially for the upper stopband and it also deteriorates the insertion loss performance when it is increased. It is very obvious in the passband since it is not only decreasing the insertion loss level but also the achieved bandwidth as demonstrated in Fig. 8. The parametric study of the last investigated parameter “ S_1 ” is clarified in Fig. 9. The spacing between the SRR and the L-stubs has a significant effect on the lower rejection band since the frequency is shifted down by about 0.2 GHz per increase of 1 mm for S_1 . Hence, the achieved passband is translated to a lower frequency range with an increased passband bandwidth but with the degraded performance of insertion loss.

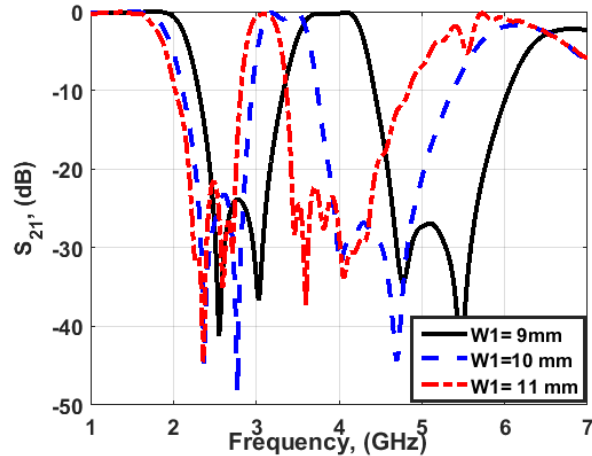


Fig. 8. The S_{21} simulated results of SRR BPF/BSF at different values ($W1$) of the SRR cell.

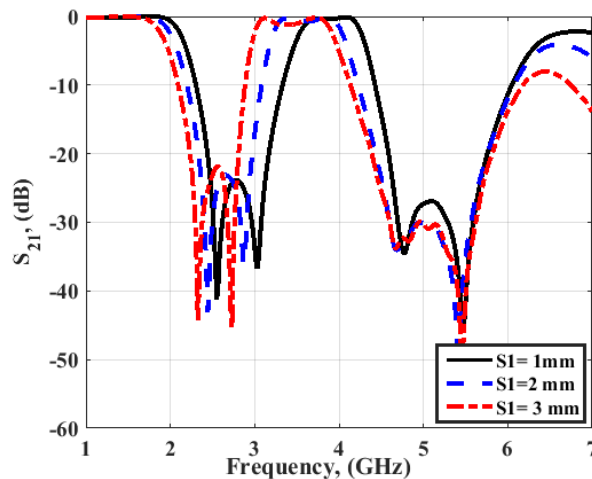


Fig. 9. The S_{21} simulated results of SRR BPF/BSF for different values of $S1$.

The surface current distribution of the suggested filter is investigated to verify the BPF performance at three resonance frequencies (3, 4, and 5 GHz). As can be observed in Fig. 10, the current is uniformly distributed from port 1 to port 2 at 4 GHz, while it is blocked at the left side of the L-stubs when it is simulated at 3 GHz and the left side of the primary SRR when it is simulated at 5 GHz.

The same performance is achieved when the electric field is investigated as in Fig. 11 confirming the ability of the suggested BPF to transfer all signals in the desired frequency band (3.5-4.3 GHz) only while rejecting all other frequencies.

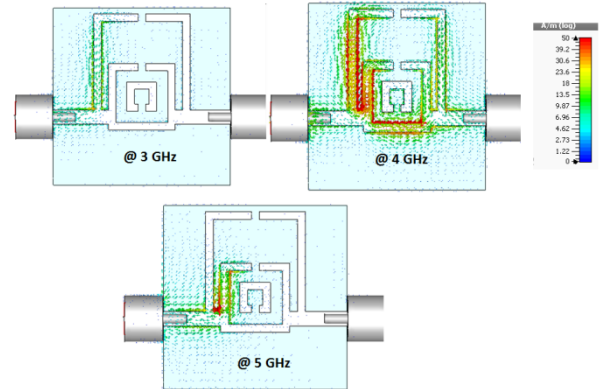


Fig. 10. The current distribution's simulated results of SRR BPF/BSF.

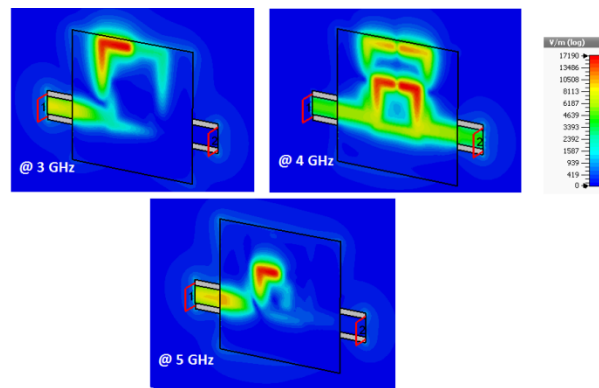


Fig. 11. The electric field distribution's simulated results of SRR BPF/BSF at $z=0.6$ mm.

IV. EXPERIMENTAL OUTCOMES

The proposed SRR-based BPF/BSF is fabricated using copper tape of the thickness of 0.1 mm and then implemented on a layer of 3-D printed PLA substrate with 3.1 dielectric constant and 2 mm thickness. Two 50-ohm SMA connectors are connected to the suggested filter through 50-ohm transmission lines as depicted in Fig. 12. The proposed filter is tested to verify its behavior using R&S ZVB 20 vector network analyzer (VNA). The simulated and measured results of return and insertion

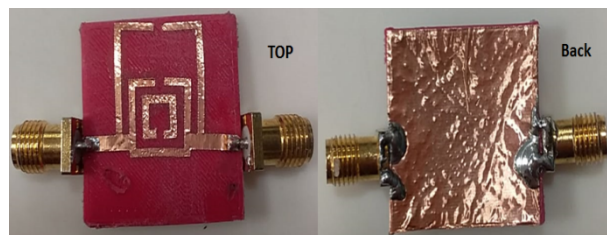


Fig. 12. The fabricated photo of the proposed SRR BPF/BSF.

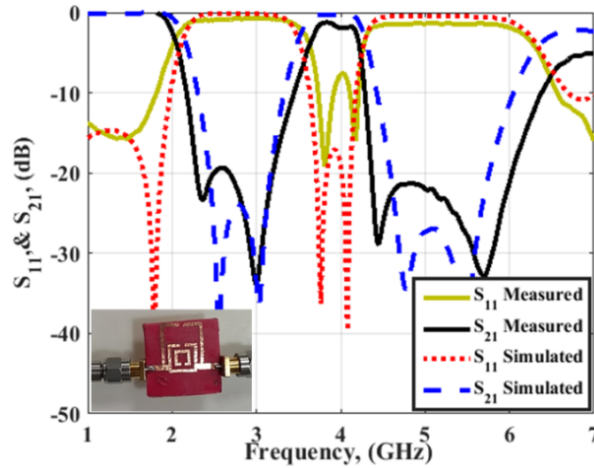


Fig. 13. The S-parameters simulated and measured results of SRR BPF/BSF.

Table 1: Comparison between proposed work and reported filters

Ref.	Response	f_o (GHz)	S_{21} (dB)	Size (λ_g)	ϵ_r/h (mm)
		FBW (%)			
[8]	Single-BPF	5.3	1.5	0.58×0.65	3.38/0.813
		8.68			
[9]	Triple-BPF	6.5/7.35 /8.15	1.74/1.82 /1.96	2.2×0.61	2.2/0.787
		2.31/2.04 /2.45			
[10]	UWB-BPF	8.35	1.5	1.28×0.36	4.4/1.6
		143			
[23]	Triple-BPF	2.5/3.4 /4.9	-	0.49×0.37	2.2/0.787
		12/21/25			
[24]	Triple-BPF	1.75/2.55 /3.55	0.55/1.36 /1.37	0.32×0.12	2.2/1.575
		21.2/4.7 /8.4			
This work	Single-BPF	3.9	1.8	0.55×0.55	3.1/1.1
		15.3			

losses are presented in Fig. 13. The BPF is operated at 3-dB bandwidth extended from 3.5 GHz to 4.3 GHz with an S_{21} level of -0.2 dB for the simulated results, while it achieves 3-dB bandwidth within 3.6 GHz to 4.2 GHz (15.3 %) with an S_{21} level of -1.8 dB for the measured results. Good consistency between the simulated and the measured results can be noticed with a slight reduction of the achieved band and this may be due to the non-

conformal stacking of the copper tape on the PLA surface and the misalignments of copper tape sections. A comparison with the recently reported work is illustrated in Table 1.

V. CONCLUSION

A compact 3-D printing BPF has been proposed. The filter has been printed on a PLA substrate. The entire size of the final filter substrate was $24 \times 24 \times 1.1$ mm³. The BPF has been operated at a 3-dB bandwidth extended from 3.4 GHz to 4.3 GHz with an S_{21} level of -0.2 dB for the simulated results while it achieves a 3-dB bandwidth within 3.6 GHz to 4.2 GHz (15.3 %) with an S_{21} level of -1.8 dB for the measured results. These outcomes enable the filter can be used in C-band applications.

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