

Design of a Miniaturized Symmetrical E-shaped MIMO Antenna with Low Coupling

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Abstract – In order to meet the demand of contemporary 5G mobile communication for miniaturized MIMO antenna systems, this paper proposes a symmetric E-shaped patch antenna. It is mainly realized by digging out the simple rectangular radiation patch, and etching four rectangular slots at the ground plane to widen the working bandwidth. The overall size of the antenna is 20 mm × 40 mm. However, there is current mutual coupling between the two radiation patches closely arranged up and down, which greatly affects the radiation effect of the antenna. Therefore, in order to reduce the coupling degree between each other, a 1 × 3 metamaterial (MTM) array structure is added between the two patches, in which the structure of the MTM unit is similar to a “concave” character. Simulation and real measurement of antennas using 3D electromagnetic simulation software HFSS and vector network analyzer, and the test results show that the proposed antenna is $S_{11} < -10$ dB in 5.32-6.02 GHz (relative bandwidth of 12.35%), the isolation degree S_{21} is above -18 dB throughout the operating frequency band, and the overall Envelope correlation coefficient (ECC) is less than 0.02 in the working band, which further confirms that the designed MIMO antenna has good isolation. The radiation pattern of the antenna is good, which is suitable for the basic requirements of 5G WLAN band.

Index Terms – E-shaped patch, high isolation, metamaterial (MTM), MIMO antenna array, miniaturization.

I. INTRODUCTION

With the development of data coding technology, wireless communication has achieved a fast data transmission rate. However, in complex propagation

environments, transmitted signals are limited by multipath fading and interference[1]. A single antenna unit can no longer meet the development needs of the communication spectrum, and MIMO antennas[2] come into being. As a new type of MIMO, it can ensure that the network bandwidth remains unchanged under the premise of exponentially increasing the capacity of the communication system and spectrum utilization[3] and, at the same time, can effectively overcome the impact of multipath and improve the communication quality and reliability of the network[4].

In recent years, character-shaped antennas have been proposed, which greatly increases the types of antennas and have a wide range of application scenarios. Back-to-back U-shaped monopole antenna [5] has a large polarization bandwidth, and some E-shaped patches have been designed. For example, an easy-to-fabricate E-shaped compact patch antenna with broadband and multi-band capabilities [6], and a triple-band E-shaped patch antenna applied to the 4G communication band [7]. However, these character antennas mentioned above are in the form of a single antenna, which cannot meet the demands of contemporary 5G communications, so the aim of this paper is to design a two-element MIMO array antenna to meet the requirements of contemporary mobile communications. In addition, current MIMO antennas focus more on performance indicators such as low coupling and high gain, while paying less attention to the miniaturization of antennas. With the continuous development of 5G wireless communication devices towards miniaturization and slimmer designs, the internal space of these devices is limited. However, miniaturized MIMO antennas[8, 9] can be better integrated into these compact devices.

Although the MIMO antenna has advantages that cannot be matched by a single antenna, it also has its own biggest drawback, that is, as a multi-input and multi-output antenna, it will produce a strong electromagnetic mutual coupling phenomenon, which will lead to the deterioration of the impedance, gain, direction diagram and other characteristics of the antenna array. How to reduce the coupling degree of the antenna while maintaining the miniaturization of the antenna is an important problem to be solved. At present, domestic and foreign scholars have put forward a variety of methods to reduce the degree of coupling, such as: adding decoupled branches, or adding artificial materials. The isolation of the miniaturized MIMO antenna by at least 10dB is improved by adding two branches to the ground and placing the MIMO antenna vertically [10]. A pair of open branch [11] was used as a decoupling network to reduce the coupling degree between the elevated antennas. Another method is to use artificial materials with special properties, such as electromagnetic band gap (EBG) [12] and metasurface [13], as decoupling structures.

Metamaterials (MTMs) are novel artificial materials that can be embedded between radiation units to improve the isolation without increasing the size and complexity of the antenna system. Literature [14–16] all uses MTM structures as decoupling structures to solve the electromagnetic coupling problem of MIMO antennas. In addition to the method introduced in this paper, the design of microstrip devices based on DMS (Defected Microstrip Structure)[17, 18] is also very common. It is in this context that this paper provides the design, simulation, and testing of a small-size, high-gain and low-coupling MIMO antenna based on MTM. In the proposed design, the improvement of isolation degree is achieved by loading a kind of “concave” shaped MTM structure. The radiating patch reduces the area of the radiating patch by digging slots, and four rectangular slots of equal length are etched on the floor to further broaden the antenna bandwidth. At this time, there is a strong electromagnetic coupling phenomenon between the two closely arranged radiating patches, in order to weaken the electromagnetic mutual coupling between the two, a certain number of MTM unit structures are added to the middle of the array. Simulation and measurement results show that the isolation of the antenna in the operating band reaches more than -18 dB after loading the MTM structure, and decoupling is achieved across the entire bandwidth after loading the MTM structure. The overall Envelope correlation coefficient (ECC) is less than 0.02 in the working band, which further confirms that the designed MIMO antenna has good isolation. The peak gain is reached at around 6 dBi. In addition, the loading of MTMs reduces the influence of sidelobe radiation of the antenna, which indicates that the antenna’s radiating performance has been optimized and enhanced with the addition of MTMs.

II. SYMMETRIC ANTENNA DESIGN PROCESS

Figure 1 shows the geometry of the two-cell compact E-shaped MIMO antenna proposed in this paper. Both patches are printed on a FR4 (dielectric constant of 4.4, dielectric loss angle tangent of 0.02) substrate with a volume of 20 mm × 40 mm × 1.6 mm. And the overall size of the antenna is very small. The antenna structure is firstly to etch the corresponding number of rectangular slots on the single rectangular patch and on the floor respectively so that the proposed single structure achieves the purpose of miniaturization of the antenna patch unit and expansion of its operating bandwidth, and finally, the single radiating patch unit is closely arranged in a symmetric way to form the MIMO two-cell antenna array structure, and the overall design steps are shown in Fig. 2. This is also the difference between the structure proposed in this paper and the previous character-based structure. During the antenna design process, the antenna structure dimensions are modeled and optimized using HFSS electromagnetic simulation software, and the final determined antenna parameters are summarized in Table 1.

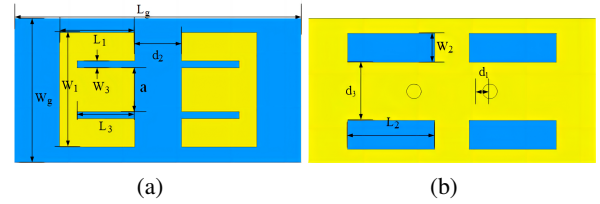


Fig. 1. The geometry of the E-shaped MIMO antenna: (a) front view and (b) back view.

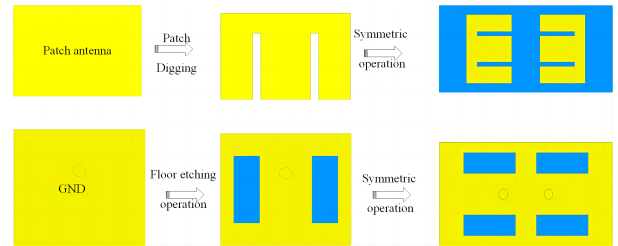


Fig. 2. Steps of the antenna design.

Table 1: Dimensions of the optimized antenna structure (unit: mm)

Parameter	Numerical Value	Parameter	Numerical Value
W_g	20	L_g	40
W_1	15.7	L_1	10.4
W_2	4	L_2	12
W_3	2.6	L_3	2
d_1	2	d_2	6.5
d_3	8	a	6

III. MTM UNIT DESIGN AND ANALYSIS

A. MTM cell design

The electromagnetic properties of artificial MTMs mainly depend on their structure and dimensions, and by designing their structure and dimensions, the metallic ohmic loss and dielectric loss near the resonance frequency can be adjusted to realize the absorption of incident electromagnetic waves. In this paper, we design a MTM unit structure that can exhibit special electromagnetic resonance characteristics near 5.8 GHz, as shown in Fig. 3. The overall size of the designed MTM structure is very small, and the parameters optimized after simulation are $a = 5.5$ mm, $c = t = t_1 = 0.4$ mm, $g_1 = 0.6$ mm, $c_1 = c_3 = 0.7$ mm, $c_2 = 2$ mm.

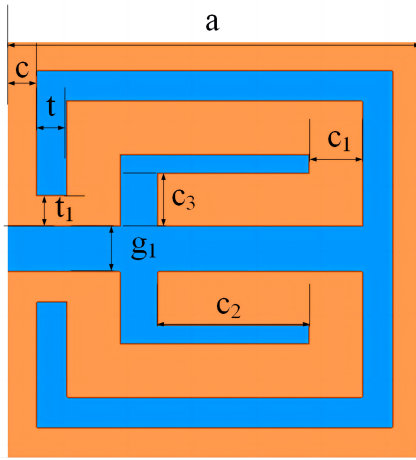


Fig. 3. MTM unit structure diagram.

In order to verify the electromagnetic characteristics of the designed MTM unit, the electromagnetic simulation software HFSS is used for detailed analysis. Open resonant circular and square rings are placed on the upper and lower surfaces of FR4 dielectric substrate with thickness of $h = 1.6$ mm, and the whole is placed in an air box. In the simulation, the upper and lower surfaces perpendicular to the z -axis are set as wave-port excitation, the front and rear surfaces perpendicular to the x -axis are set as ideal magnetic conductors (Perfect H), and the left and right surfaces perpendicular to the y -axis are set as ideal electric conductors (Perfect E). At this time, the magnetic field is perpendicular to the surface of the MTM cell, which is used to simulate the generation of the magnetic resonance when the magnetic field passes through the cell, as shown in Fig. 4.

B. Simulation analysis

The MTM is characterized by a normally incident X-polarized wave and a scattering parameter extracted from a single unit cell with periodicity. In order to obtain

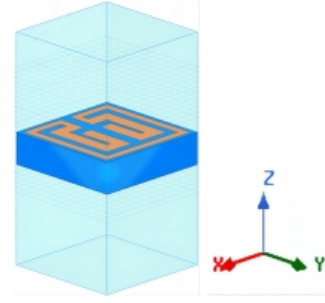


Fig. 4. A 3D view of the MTM cell structure.

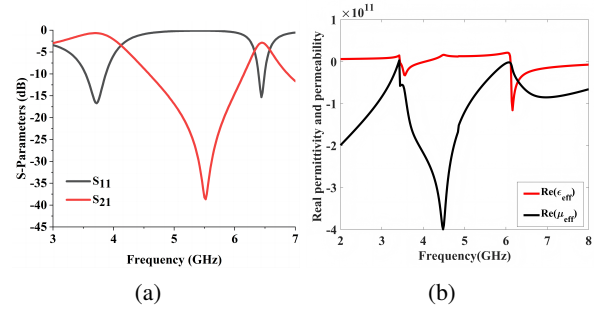


Fig. 5. (a) Plot of the S-parameter structure and (b) plot of the extracted equivalent parameter values.

the characteristic parameters of the MTM, the S parameter inversion method [19, 20] is needed. Figures 5 (a) and (b) show the magnitude of the S-parameter of the MTM cell structure and the equivalent parameter values of its permeability and permittivity, respectively. From the results, it can be seen that the value of its equivalent magnetic permeability μ at 5-6 GHz is negative, and the value of the equivalent permittivity ϵ is positive, which can indicate that the MTM is an electronegative material. It can be observed from the transmission and reflection characteristics that the MTM has a determined suppression bandwidth between 5-6 GHz, especially a transmission stop band due to magnetic resonance near the center frequency point 5.8 GHz. It can be used to suppress the propagation of coupling current from one antenna element to another to improve isolation between antenna array elements.

IV. ANALYSIS OF THE OVERALL MIMO ANTENNA STRUCTURE AND THE EXPERIMENTAL RESULTS

The purpose of decoupling is achieved by loading the 1×3 MTM array structures between the two radiation patches, and the overall antenna structure is shown in Fig. 6. To make the measurements comparable, the original and loaded MTM antennas adopt the same structural dimensions, where $d_3 = 0.4$ mm, $d_4 = 0.5$ mm.

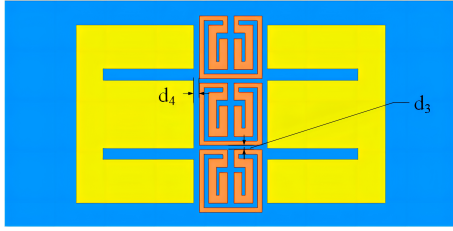


Fig. 6. Front view of the integral MIMO antenna loaded with MTMs. (Blue is the dielectric substrate, the radiation patch is yellow and the MTM structure on the same surface as the radiation patch is orange).

A. S-parameter simulation analysis

Figure 7 is a comparison diagram of the antenna S-parameters obtained by the HFSS software simulation. Figure 7 (a) shows that the central working frequency of the MIMO antenna loaded with MTMs is slightly shifted to the low frequency, but the overall deviation of the working frequency band is not large. It can be seen from Fig. 7 (b) that by loading MTMs, the coupling coefficient S_{21} obtained a substantial decrease of the MIMO antenna in the entire working frequency band. Compared with the original antenna, the coupling degree not only achieves the minimum requirement of the MIMO antenna but also achieves a maximum of 10 dB decoupling, and the coupling reduction effect is remarkable.

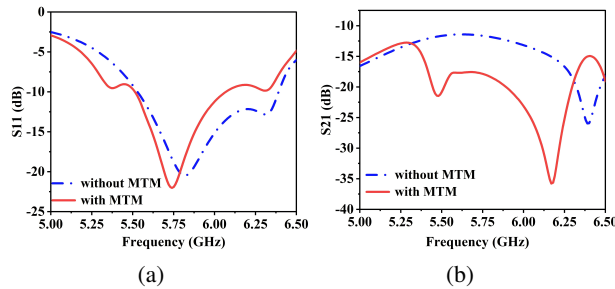


Fig. 7. S-parameter plot of the antenna: (a) S_{11} and (b) S_{21} .

B. 2D radiation pattern

Figure 8 shows a comparison of the two-dimensional far-field radiation pattern of the antenna before and after loading the MTM structure in the E-plane and H-plane at 5.8 GHz. As can be seen from the comparison figures, compared with the ordinary MIMO antenna, the directional map of two-dimensional far-field radiation in the H-plane of the MIMO array antenna loaded with MTMs is unchanged, indicating that the introduction of the MTMs does not damage the far-field radiation characteristics of the antenna. In addition, it can be seen from Fig. 8 (a) that adding MTM enhances

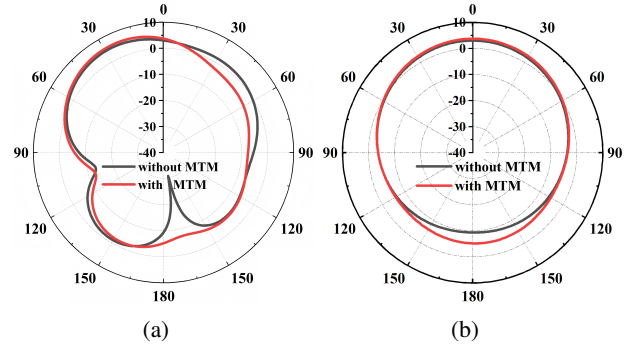


Fig. 8. Radiation pattern of the antenna with and without MTM: (a) E-plane and (b) H-plane.

the main flap radiation of the far-field radiation of the antenna's E-plane more obviously. That is, the MIMO antenna without MTM produces large side lobe radiation between 120 and 180 degrees. Instead, the MIMO antenna with MTM produces strong main lobe radiation in the direction of 150 degrees. The side lobe radiation at this time is very small, which further indicates that the MTM structure has a significant role in improving the performance of the MIMO antenna.

C. Antenna surface current distribution

In order to understand the decoupling principle of the loaded MTM antenna more intuitively, the surface current distribution of the antenna before and after the loading of the MTM is analyzed at the center frequency point of 5.8 GHz, and the comparison results are shown in Fig. 9. In order to make a visual comparison, the same current intensity scale has been chosen for both figures, with darker colors (red) indicating a denser distribution of current intensity on the surface, and lighter colors (blue) indicating a sparser distribution of current intensity on the surface, where the left figure is the case not based on MTMs, and the right figure is the case based on MTMs. From the comparative analysis of the left and right figures, it can be seen that the surface current strength distribution on the antenna array element in the left figure is denser, which can produce stronger coupling to the neighboring antenna array elements, whereas in the right figure, after the addition of the MTM structure in the middle of the two antenna units, the surface current strength distribution on the following antenna array element becomes obviously sparse, which further indicates that the designed MTMs can effectively weaken the electromagnetic mutual coupling between two closely spaced antenna elements.

D. 3D radiation gain direction map of the antenna

A comparison of the 3D radiation gain directional map of the antenna at the center frequency point 5.8 GHz

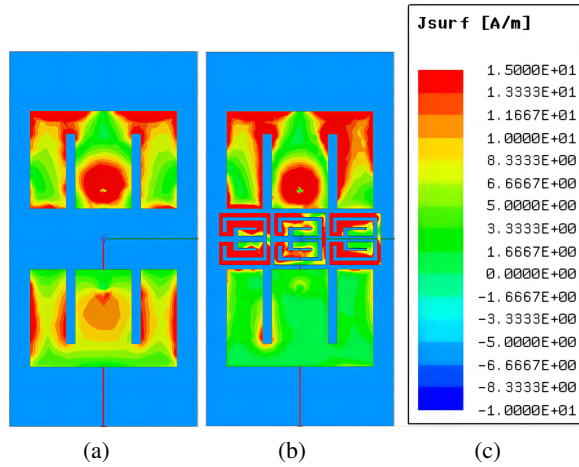


Fig. 9. Surface current map at 5.8 GHz: (a) without MTMs, (b) with MTMs and (c) current intensity distribution.

generated in the electromagnetic simulation software is shown in Fig. 10. From the figure, it can be seen that the addition of the MTM has an effect on the antenna gain, that is, it increases the antenna gain by a small amount, with an overall increase of 1.05 dB. From the 3D radiation gain direction map, the highest gain of the antenna reaches 5.89 dB, which meets the range requirements of 5G mobile communication antennas for high gain.

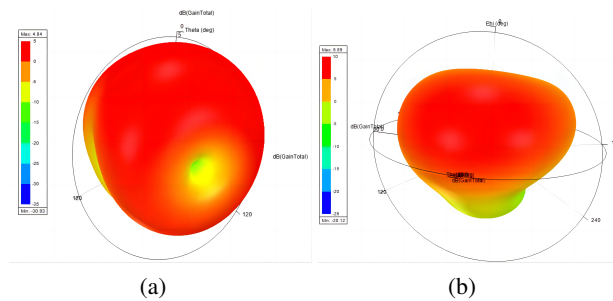


Fig. 10. 3D gain orientation diagram: (a) without MTMs and (b) with MTMs.

E. Gain and efficiency of proposed antenna

Figure 11 shows the resulting plot of the gain and efficiency of the MIMO antenna after loading the MTM. We can see from the figure that the peak gain ranges from 4.08 dBi to 5.95 dBi. The radiation efficiency ranges from 66% to 80% in the entire operating frequency band, and the radiation efficiency at the center frequency of 5.8 GHz is about 80%. The maximum gain is 5.95 dBi at 5.9 GHz and the minimum gain is 4.08 dBi at 5.36 GHz.

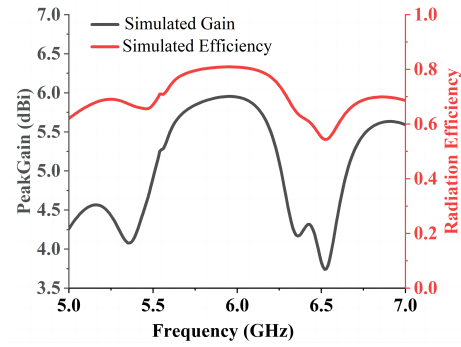


Fig. 11. Gain and efficiency of proposed antenna.

F. The MIMO antenna diversity characteristics

ECC and diversity gain are the two most important parameters to show the diversity characteristics of MIMO antenna. Figure 12 presents the simulated ECC and diversity gain diagram of MIMO antenna. It can be seen from the figure that the ECC value meets the minimum requirements of the ideal value in the entire working band, and the overall ECC is less than 0.02 in the working band. This confirms that the designed MIMO antenna has good isolation and the best performance under a multipath fading environment. Moreover, in the working frequency band, the proposed MIMO antenna achieves a diversity gain of 10 dBi with good diversity characteristics.

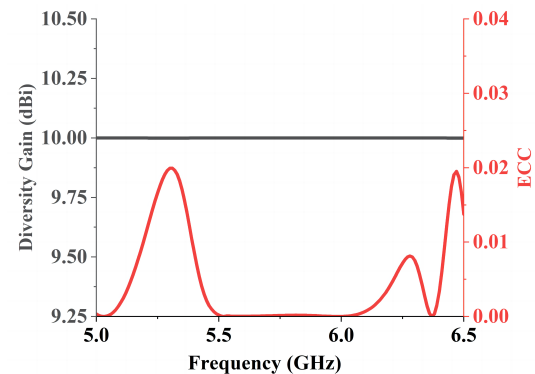


Fig. 12. Gain and efficiency of proposed antenna.

G. Comparative analysis of antenna array elements

The MIMO antenna arrays presented in Table 2 have similarities in shape, and their performance is compared in this section. Compared with [21–23], the structure in this paper has advantages in isolation and gain although the bandwidth is relatively narrower. Although the design has disadvantages in isolation compared with [24–26], the operating bandwidth is relatively wider. Compared with these four antenna arrays,

Table 2: Comparison between the proposed antenna and other antennas

Ref	Electrical Dimensions	Center Frequency Point (GHz)	Bandwidths (GHz)	Isolation (GHz)	Gain (GHz)
[21]	$0.57\lambda_0 \times 0.385\lambda_0$	6, 8, 10	5.2-10.6 (68.35%)	<-15	5.7
[22]	$1.07\lambda_0 \times 1.07\lambda_0 \times 0.01\lambda_0$	2.3, 2.5, 2.65	2.22-2.75 (21.3%)	<-18	5.5
[23]	$0.44\lambda_0 \times 0.5\lambda_0$	3.5	3.22-4.36 (30.07%)	Not Given	5.2
[24]	$0.81\lambda_0 \times 0.5\lambda_0 \times 0.02\lambda_0$	2.45	2.449-2.456 (0.29%)	<-22	6.68
[25]	$0.4\lambda_0 \times 0.61\lambda_0 \times 0.01\lambda_0$	2.77	2.73-2.85 (4.3%)	<-50	Not Given
[26]	$0.84\lambda_0 \times 1.01\lambda_0$	3.5	3.5-3.55 (1.42%)	<-20	Not Given
This paper	$0.66\lambda_0 \times 0.33\lambda_0 \times 0.02\lambda_0$	5.8	5.32-6.02 (12.35%)	<-18	5.89

the antenna structure has a greater advantage in terms of small size, which is better able to meet the demand of modern mobile devices on the antenna miniaturization. In addition, the comparison of the electrical dimensions of the antennas is more reflective of the smaller dimensions of the proposed antennas. Therefore, the design can meet the most basic requirements of the antenna in high isolation, small size, broadband and high gain.

V. ANTENNA FIELD MEASUREMENT AND RESULT

To validate the proposed design, an antenna prototype was made and measured. The antenna was simulated using ANSYS HFSS. The antenna made according to the above parameters is shown in Fig. 13, and the S parameter of the antenna was measured using the Network Analyzer (NA). The measured and simulated values of the S parameters are shown in Fig. 14. Comparing the simulation results and the measured results, we find that there is a small frequency shift. This may be due to factors such as SMA connector loss, cable loss, and radiation boundary during measurement. The measured results show that the measured frequency band of the proposed MIMO antenna of $S_{11} < -10$ dB is basically

unchanged and $S_{21} < -20$ dB. And the measured and simulation results are generally moderate.

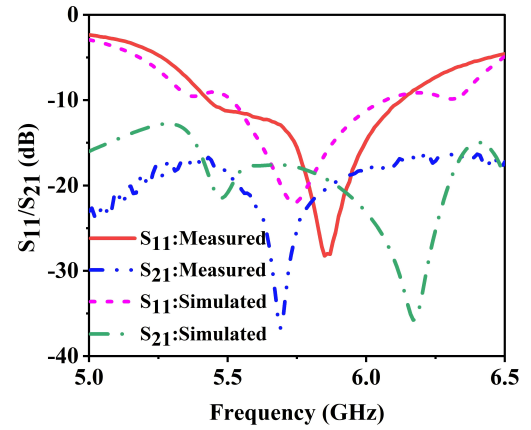


Fig. 14. Measured and simulated S-parameters of the designed MIMO antenna.

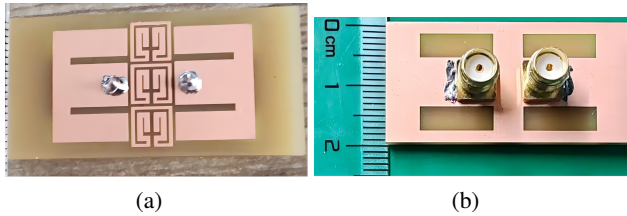
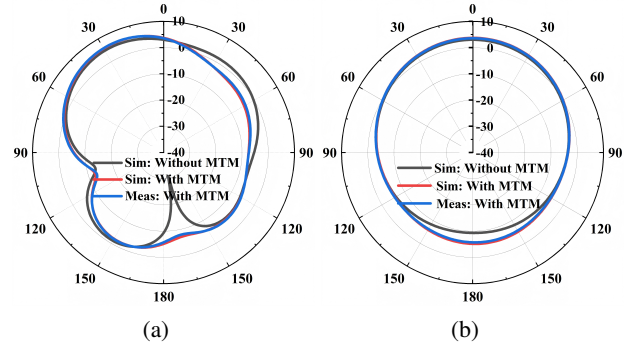


Fig. 13. Physical representation of an antenna loaded with MTMs: (a) front view and (b) back view.


 Fig. 15. Measured and simulated radiation pattern (with or without MTMs) at 5.8 GHz: (a) $\Phi = 0^\circ$ and (b) $\Phi = 90^\circ$.

Next, the radiation characteristics of MIMO antenna in both cases (with or without MTMs) were further studied. Figure 15 shows the simulation and measured radiation pattern of the main plane azimuth ($\Phi = 0^\circ$) and pitch ($\Phi = 90^\circ$) at 5.8 GHz, which shows that the introduction of the MTM has a slight effect on the deviation of the radiation pattern.

VI. CONCLUSION

In this paper, a symmetric “E-shaped” MIMO dual-cell array antenna for 5G WLAN band is proposed by combining the character-shaped radiating patch and MIMO technology to optimize the shortcomings of a single patch antenna, such as low spectrum utilization. A kind of “concave” shaped MTM cell structure is proposed to improve the isolation degree between two antenna cells, which is mainly placed between two radiating patches in a 1×3 arrangement. The distance from the MTM array structure to the two patch cells can be adjusted to reduce the coupling degree between the MIMO antenna array cells. Comparison of the measured and simulated results shows that the introduction of MTM improves the impedance matching characteristics of the antenna array compared with the original antenna and steadily improves the gain of the antenna. Although the gain improves less, the overall gain meets the minimum requirements of high gain. Meanwhile, the isolation degree is above -18 dB throughout the operating frequency band, and achieves a maximum of 10 dB decoupling compared to the antenna array without MTM. Compared with the same type of antenna, the antenna has some advantages in terms of miniaturization, gain and isolation. Therefore, the proposed MIMO antenna system is suitable for the field of miniaturized MIMO dual array antennas with high isolation.

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