Single Layer Reflectarray Antenna with Pie-Shaped Elements for X-band Applications

Tayyab Shabbir¹, Rashid Saleem¹, Sabih U. Rehman², and Muhammad Farhan Shafique³

¹Department of Telecommunication Engineering University of Engineering and Technology, Taxila, 47050, Pakistan {Tayyab.Shabbir, Rashid.Saleem}@uettaxila.edu.pk

² School of Computing and Mathematics, Charles Sturt University, Australia sarehman@csu.edu.au

³Center for Advanced Studies in Telecommunication COMSATS University Islamabad, Park Road, Tarlai Kalan, Islamabad, 45550, Pakistan Farhan.Shafique@comsats.edu.pk

Abstract – In this paper, a single-layer reflectarray design is presented for X-band applications. The reflectarray comprises of pie-shaped reflective elements. The unit element has compact dimensions of $0.28\lambda_o \times 0.28\lambda_o$. The major segment angle of pie-shaped element controls the reflection phase range and offers a total of 650° phase variation. A reflectarray prototype comprising 23×23 elements is realized to demonstrate the necessary reflection characteristics. Different parameters are analyzed for performance evaluation of the reflectarray. The proposed reflectarray offers measured gain of 24 dBi with 1-dB and 3-dB gain bandwidth of 18% and 28% respectively. Moreover, side-lobe-levels and cross-polarizations are less than 22 dB and 35 dB respectively.

Index Terms — Radiation patterns, reflectarray antenna (RA), reflection magnitude, reflection phase range.

I. INTRODUCTION

Among various modules of high-speed transceivers, the RF front-end has gained considerable attention over the last two decades. High gain antennas, being the crucial part of front-end, play an important role in long distance communication and other applications like remote sensing. Conventionally, parabolic reflectors and phased-arrays are used for high gain applications. Parabolic reflectors are difficult to realize owing to their curved geometry and phase arrays on the other hand have complicated and lossy feed networks. The phased-arrays and parabolic reflectors can be effectively substituted by reflectarrays. The reflectarrays offer certain advantages over parabolic reflectors as well as phase arrays by combining the features of these two high gain antenna classes. Reflectarrays are low cost, light weight and easy to fabricate and deploy. Reflectarrays have multiple reflective elements printed on a substrate, backed by a ground plane and illuminated by a feed horn antenna. The operating principle of reflectarray is illustrated in Fig. 1. Overall, one of the common limitations of reflectarrays is their narrow operating bandwidth. However, their bandwidth can be improved by employing elements with a broad linear phase range [1 - 3].

Recently, different techniques are proposed to control the reflection phase of reflectarrays. These techniques include but are not limited to variation in geometrical parameters, variable size patches, identical elements with different rotation angles etc. In [4], a modified cross loop reflectarray is presented. A wide phase range of 550° is achieved by varying the length of cross shape. A fractal reflectarray of first and second order with phase range of 354° is presented in [5]. A slotted hollow ring with stacked ground plane is presented recently where the desired gain is achieved by rotating the slotted ring [6]. In [7], a square shaped reflectarray attached with lattice stubs is reported. The stub length is optimized to achieve a broad phase variation of 600°. Parallel dipoles based reflectarray for high gain and broad phase range of 413° is presented in [8]. A single layer qausi-spiral reflectarray with small dispersion in transmission modes is presented in [9]. It is envisioned that the phase range can be further enhanced to improve the design bandwidth with simple geometry and single layer realization as compared to the existing literature.

In this article a single layer pie-shaped reflectarray for X-band applications is proposed. The reflectarray is designed and optimized using a commercially available 3D full-wave electromagnetic solver based on Finite Element Method (FEM) algorithm (Ansys HFSS). The outline of the paper is as follows: unit element design is presented in Section II. The reflectarray configuration and measurement setup is elaborated in Section III. Finally, Section IV concludes the paper.



Fig. 1. Reflectarray operational principle.

II. UNIT ELEMENT DESIGN AND ANALYSIS

Unit element is designed and optimized for X-band applications with centre frequency of 10 GHz. The reflectarray unit element geometry is shown in Fig. 2. The design has compact dimensions of $0.28 \lambda_o \times 0.28 \lambda_o$, where λ_o is free space wavelength at 10 GHz. The reflectarray is designed on FR-4 substrate with dielectric constant of 4.4 and a loss tangent of 0.02. The top-layer comprises of pie-shaped unit element and the ground plane is placed on the flip side of substrate. The unit element optimized parameters for 10 GHz are shown in Table 1.



Fig. 2. Reflectarray unit element configuration.



Fig. 3. Unit element measurement through waveguide simulator method.

Table 1	:	Unit cell	0	ptimized	parameters	at	10	GHz

Parameter	D _Y	D _X	R	G	Т
Value (mm)	8.5	8.5	4	0.25	1.6

A. Unit cell performance parameters

The parametric analysis for simulated reflection magnitude against frequency is shown in Fig. 4. The reflection curve moves towards lower frequencies when the major segment angle of pie-shaped element, ϕ_s , is increased and vice versa. Moreover, reflectarray unit cell prototype for 10 GHz frequency is fabricated, as shown in Fig. 3 and reflection magnitude is measured through waveguide simulator method.



Fig. 4. Reflection magnitude at different segment angles.

The phase range is examined over different parameters, i.e., oblique incident angles in transmission modes and different frequencies. The phase range at 9, 10 and 11 GHz is shown in Fig. 5. By varying the major segment angle, ϕ_s , from 0° to 350°, the design achieves a phase range of 650°. The simulated phase range for TE and TM modes at different oblique incident angles is shown in Figs. 6 (a) and 6 (b). A stable phase response with little shift is obtained at 30° and 45° oblique incident

angles, which is within acceptable limits [10]. Conventionally, the value of real part of impedance should be higher to avoid losses in the reflectarray. The real and imaginary parts of impedance are shown in Fig. 7. The real part of impedance (resistance) is more than 2000 Ω at 10 GHz frequency [11].



Fig. 5. Reflection phase range at 9, 10 and 11 GHz.



Fig. 6. Performance parameters effect on phase range.



Fig. 7. Input impedance at 10 GHz.

III. REFLECTARRAY REALIZATION AND MEASUREMENT SETUP

A 23×23 element reflectarray is designed on FR-4 substrate. The reflectarray panel has dimensions of $6.5\lambda_o$ $\times 6.5\lambda_o$, where λ_o is the free space wavelength at 10 GHz. The array elements are equally spaced with inter-element spacing of $0.28\lambda_o$. The spacing between elements is commonly kept less than $0.5\lambda_o$, to reduce the presence of grating lobes [1]. Generally, in array configuration, a minor change in the size of unit element produces a large phase shift in the reflected wave. The required phase distribution on each element in reflectarray is attained by using Equation 1:

$$\phi_R = K_o(d_i - (x_i \cos \phi_o + y_i \sin \phi_o) \times \sin \theta_o). \quad (1)$$

The parameters used in array Equation (1) are elaborated in [1, 12]. The phase distribution plot is used to calculate the opening angle of each array element. The phase distribution on center-fed pie-shaped reflectarray is depicted in Fig. 8 (a). A stronger phase shift is observed at the center than at the corners/sides. The ratio of focal length to diameter of reflectarray is defined as F/D ratio. The fabricated pie-shaped reflectarray has an F/D ratio of 1. Reflectarrays have electrically large aperture size and require high computational resources and time. Therefore, a hybrid Finite Element Boundary Integral (FEBI) algorithm is used for reflectarray system simulations. This algorithm combines the Finite Element Method (FEM) with Integral Equation (IE) method [12]. This method efficiently handles the complex and electrically large sized structures. The reflectarray farfield radiation characteristics are obtained by using hybrid FEBI method. Full reflectarray simulations with feed horn and 23×23 reflectarray elements were performed on a ten-core HP Z840 workstation with workable memory of 64 GB. The CPU took about 23 hours to fully simulate the reflectarray. The reflectarray antenna FEBI system model as shown in Fig. 8 (b) is used to obtain far field characteristics.



(b) Reflectarray system modeling with FEBI algorithm

Fig. 8. Reflectarray system model along with phase distribution.

The fabricated reflectarray antenna and the measurement setup is shown in Fig. 9. The fabricated 23×23 elements reflectarray on FR-4 laminate is placed inside a wooden stand and illuminated by an X-band WR-90 feed horn antenna. The feed horn is placed 194 mm away from the center of array panel. The reflectarray antenna measurements are carried out in an anechoic chamber.

The simulated and measured E and H-plane radiation patterns at 10 GHz are shown in Fig. 10. The side-lobelevels and cross polarizations are less than 22 dB and 35 dB for the reflectarray. The gain against frequency is shown in Fig. 11. A gain of 24 dBi with aperture efficiency of 48% is achieved at 10 GHz. Moreover, 1-dB and 3-dB gain bandwidths are 18% and 28% respectively. The proposed reflectarray comparison with previously reported reflectarrays is listed in Table 2.



(a) Fabricated 23×23 element reflectarray



(b) Reflectarray under testing

Fig. 9. Fabricated reflectarray and measurement setup.

Table 2: Comparison with previously reported reflectarrays

References	This Work	[15]	[14]	[13]	[12]	
Middle						
frequency	10	12.5	10	13.5	10	
(GHz)						
Gain (dBi)	24	26.6	26.1	24.5		
Aperture						
efficiency	48	52.5	40.3	39	49.5	
(%)						
1-dB						
bandwidth	18	8.1	18	20	12.5	
(%)						
3-dB						
bandwidth	28	19.8	30		34	
(%)						
Side-lobe-levels	22		16	25	35	
(dB)	-22		-10	-25	-33	
X-pol (dB)	-35	-21	-23	-30	-40	



Fig. 10. E and H-plane gain patterns at 10 GHz.



Fig. 11. Gain vs. frequency.

VI. CONCLUSION

Pie-shaped reflectarray for X-band is presented in this paper. Reflectarray prototype of size $6.5\lambda_o \times 6.5\lambda_o$ is fabricated with an *F/D* ratio of 1. The reflectarray performance is analyzed in terms of reflection magnitude, phase range, TE and TM modes. The reflectarray has a measured gain of 24 dBi at 10 GHz frequency. The simulated results are in good agreement with the measured results. The results strongly suggest that the reflectarray is a suitable candidate for high gain X-band applications.

REFERENCES

- [1] P. Nayeri, F. Yang, and A. Z. Elsherbeni, "Beamscanning relectarray antennas: A technical overview and state of the art," *IEEE Antennas and Propagation Magazine*, vol. 57, no. 4, pp. 32-47, 2015.
- [2] J. Shaker, M. R. Chaharmir, and J. Ethier, *Reflectarray Antennas: Analysis, Design, Fabrication, and Measurement.* Artech House, 2013.
- [3] B. Honarbakhsh, "FR4-only microstrip reflectarray antennas for 5.8 GHz dual-polarized wireless bridges," *Applied Computational Electromagnetics Society Journal*, vol. 31, no. 4, pp. 355-360, 2016.
- [4] Q. Wang, Z. Shao, P. Li, L. Li, and Y. Cheng, "A dual polarization, broadband millimeter-wave reflectarray using modified cross loop element," *Microwave and Optical Technology Letters*, vol. 56, no. 2, pp. 287-293, 2014.
- [5] S. Costanzo and F. Venneri, "Miniaturized fractal reflectarray element using fixed-size patch," *IEEE Antennas and Wireless Propagation Letters*, vol. 13, pp. 1437-1440, 2014.
- [6] H. Chen, G. Zhang, X. Lei, and J. Wu, "A slotted hollow ring element for Ku-band high-efficiency circularly polarized reflectarrays," *Microwave and Optical Technology Letters*, vol. 57, no. 11, pp. 2629-2632, 2015.
- [7] S. F. Qotolo, H. R. Hassani, and M. Naser-Moghadasi, "A novel broadband reflectarray antenna with lattice stubs on square element for Ku-band application," *Microwave and Optical Technology Letters*, vol. 57, no. 11, pp. 2699-2702, 2015.
- [8] J. H. Yoon, Y. J. Yoon, W. S. Lee, and J. h. So, "Broadband microstrip reflectarray with five parallel dipole elements," *IEEE Antennas and Wireless Propagation Letters*, vol. 14, pp. 1109-1112, 2015.
- [9] I. Derafshi, N. Komjani, and M. Mohammadirad, "A single-layer broadband reflectarray antenna by using quasi-spiral phase delay line," *IEEE Antennas and Wireless Propagation Letters*, vol. 14, pp. 84-87, 2015.
- [10] E. R. F. Almajali and D. A. McNamara, "Angle of incidence effects in reflectarray antenna design: Making gain increases possible by including incidence angle effects," *IEEE Antennas and Propagation Magazine*, vol. 58, no. 5, pp. 52-64, Oct. 2016.
- [11] F. Costa and A. Monorchio, "Closed-form analysis of reflection losses in microstrip reflectarray antennas," *IEEE Transactions on Antennas and Propagation*, vol. 60, no. 10, pp. 4650-4660, Oct.

2012.

- [12] T. Shabbir, R. Saleem, S. U. Rehman, and M. F. Shafique, "A compact single layer reflectarray antenna based on circular delay-lines for X-band applications," *Radioengineering*, vol. 27, no. 2, pp. 440-447, 2018.
- [13] S. F. Qotolo, H. R. Hassani, and M. Naser-Moghadasi, "A novel broadband reflectarray antenna with lattice stubs on square element for ku-band application," *Microwave and Optical Technology Letters*, vol. 57, pp. 2699-2702, 2015.
- [14] J. Wu, X. Da, and K. Wu, "Circularly polarized high efficiency wideband reflectarray using rectangle-shaped patch element," *International Journal of RF and Microwave Computer Aided Engineering*, vol. 27, no. 5, 2017.
- [15] X. Da, J. Wu, J. Zhao, L. Baoqin, and K. Wu, "Single-layer circularly polarized wide band reflectarray antenna with high aperture efficiency," *International Journal of Antennas and Propagation*, vol. 2018, Article ID 2403052, 2018.



Tayyab Shabbir received his B.Sc. in Electrical Engineering in 2011 from COMSATS Institute of Information Technology, Islamabad, Pakistan and Masters in Telecommunication Engineering in 2014 from University of Engineering and Technology (UET) Taxila, Pakistan,

where he won a studentship. Recently he is again awarded a Ph.D. studentship by UET Taxila. His main research interests are in reflectarrays, Frequency Selective Surfaces and UWB-MIMO systems.



Rashid Saleem received B.S. Electronic Engineering from Ghulam Ishaq Khan Institute of Engineering Sciences and Technology, Pakistan, in 1999. He pursued a career in the telecommunication industry for several years while continuing education. He received M.S. from

UET Taxila through Center for Advanced Studies in Engineering, Pakistan, in 2006 and Ph.D. from The University of Manchester, United Kingdom in 2011. In his Ph.D., he worked in Microwave and Communication Systems research group under the supervision of Prof. Anthony K. Brown, then-head of the School of Electrical and Electronic Engineering, The University of Manchester. He worked on antennas, channel modeling and interference aspects of Ultra-Wideband systems during his Ph.D. and was also member of a team designing and testing arrays for the Square Kilometer Array project. Currently, he is working as Assistant Professor at University of Engineering and Technology (UET), Taxila, Pakistan where he is supervising several postgraduate students and heading the MAP (Microwaves, Antennas and Propagation) research group. His research interests include antennas, angle-of-arrival based channel modeling, microwave periodic structures and metamaterials.



Sabih Ur Rahman is Adjunct Lecturer in the School of Computing and Mathematics at Charles Sturt University, Australia. He has combined experience in the field of Telecommunication and Information Technology for over 16 years in both enterprise and educational sector

environments. Sabih completed his Ph.D. from Charles Sturt University, in the area of Vehicular Wireless Communication in 2016. He received his Bachelor's degree from University of South Australia, Adelaide in Electronics & Telecommunication Engineering with Honours. Sabih is also the recipient of a competitive scholarship from Charles Sturt University for his doctorate. Sabih's current research interests are in the areas of antennas and propagation.



Muhammad Farhan Shafique received B.Eng. degree from Hamdard University, Karachi, Pakistan, in 2003, M.S. degree from the University of Paris East Marne-la-Vallée, Paris, France, in 2005 and Ph.D. in Electronic and Communications Engineering from The University of

Leeds, Leeds, U.K in 2010. In 2005, he was an Intern at Conservatoire national des arts et métiers, Paris, France. From 2007 to 2010 he was involved in establishing the LTCC fabrication facility at Institute of Microwave and Photonics, The University of Leeds, UK. His research interests involve multilayered-microwave device fabrication on LTCC and thick-film technology, RF antenna and antenna arrays, Ultra-Wideband diversity antennas and MEMS packaging. He is also involved in dielectric characterization of materials using microwave techniques and fabrication of ceramic microfluidic devices. He is the founding head of Microwave Components and Devices (MCAD) research group, Associate Professor and Associate Director at Center for Advanced Studies in Telecommunications (CAST).